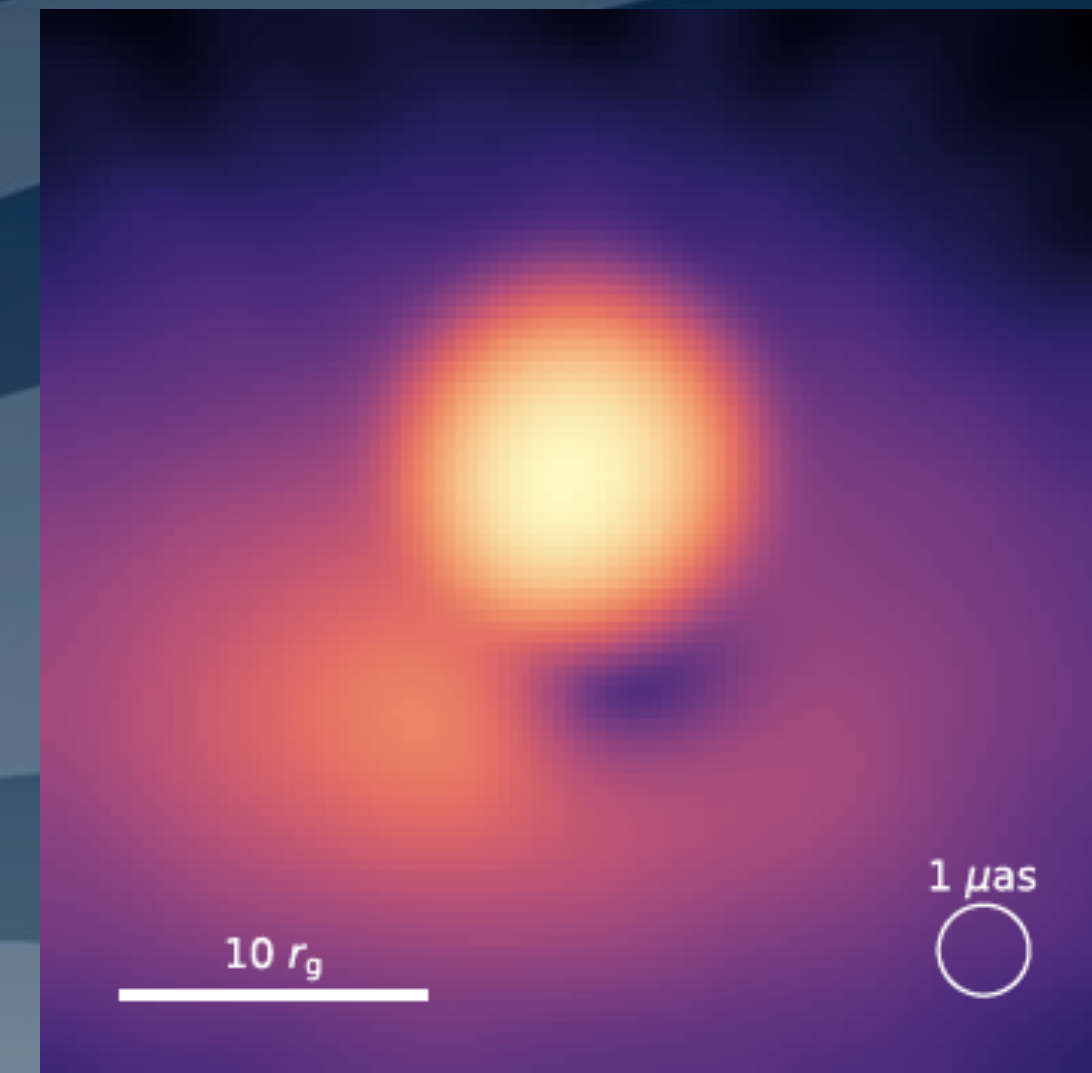
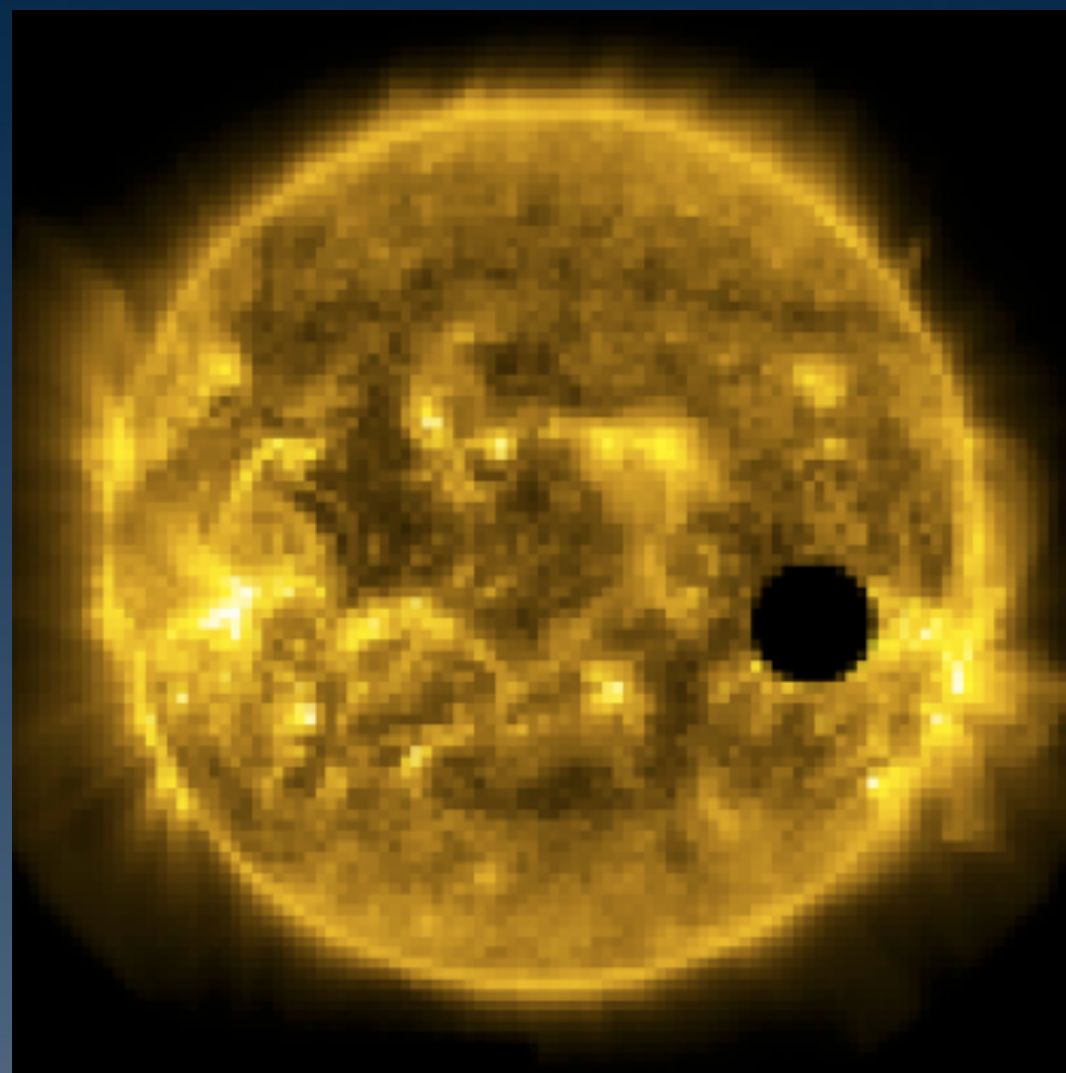


Astrophysics with Diffraction-Limited X-ray Optics



MAXIM (Cash+ '00) and MAXIM Pathfinder (Gendreau+ '02)
 Multilayer-based, normal incidence optics (Windt & Kahn '03)
 MASSIM diffraction/refraction optics (Skinner+ '08)
 New: Micro-Arcsecond X-ray Optics Concept: (Chalifoux+, in prep.)
 X-ray Interferometry for ESA Vision 2050: (Uttley et al. '19)

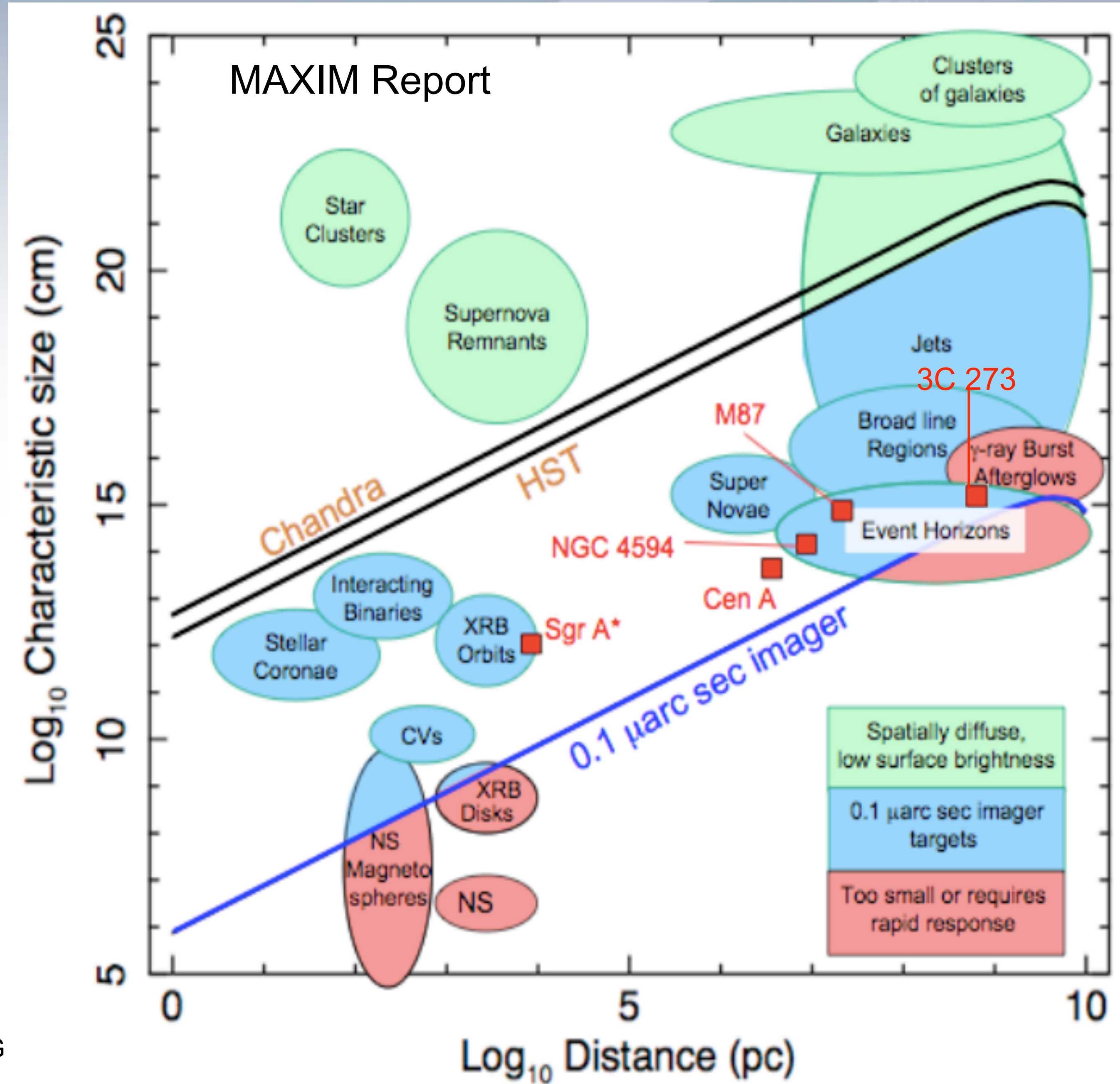
The Plan



- Scientific Motive
 - Imaging AGN and XRB black hole accretion disks, planetary systems
 - High temperatures mean high brightness and small angular sizes
- Technical Issues
 - Diffraction-limited optics
 - Formation flying
 - Small pixel detectors
 - System metrology & active alignment
 - Attitude control and knowledge
- Strategy and Progress
 - EUV lithography yields diffraction-limited optics
 - Si mirrors are nearly there for X-ray optics
 - CMOS detectors reduce formation flying requirements
 - Active alignment and mas-level control being tested in small systems
 - Staged development: $0.05'' \Rightarrow 0.000,1'' \Rightarrow 0.000,000,1''$

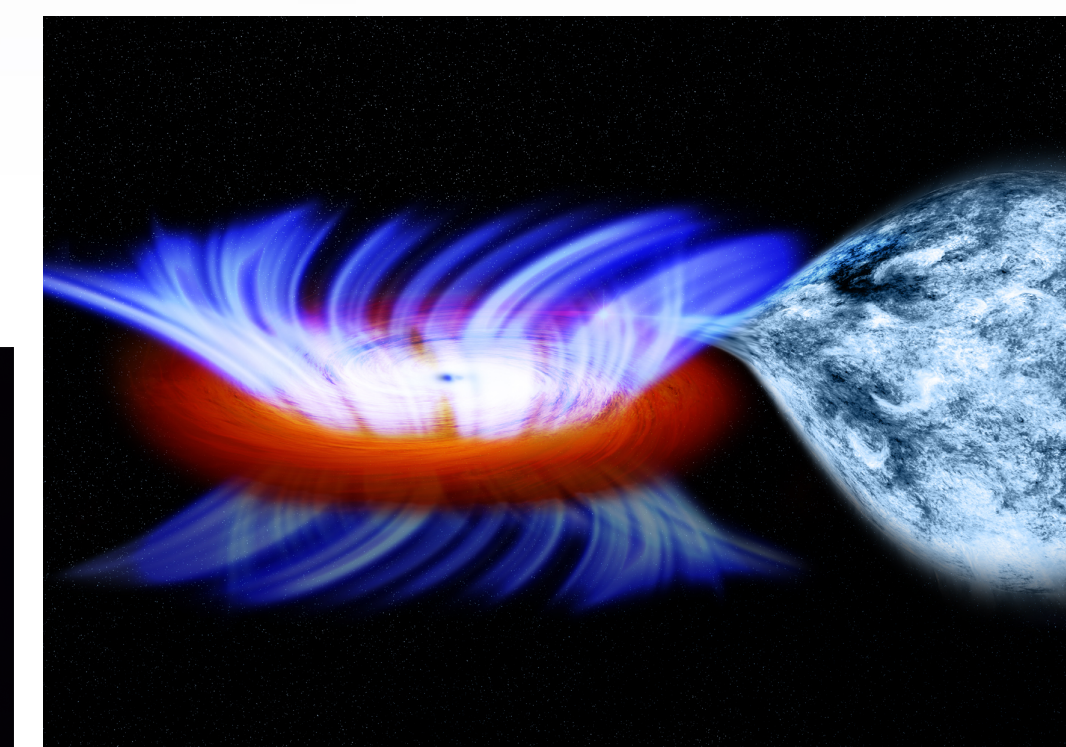
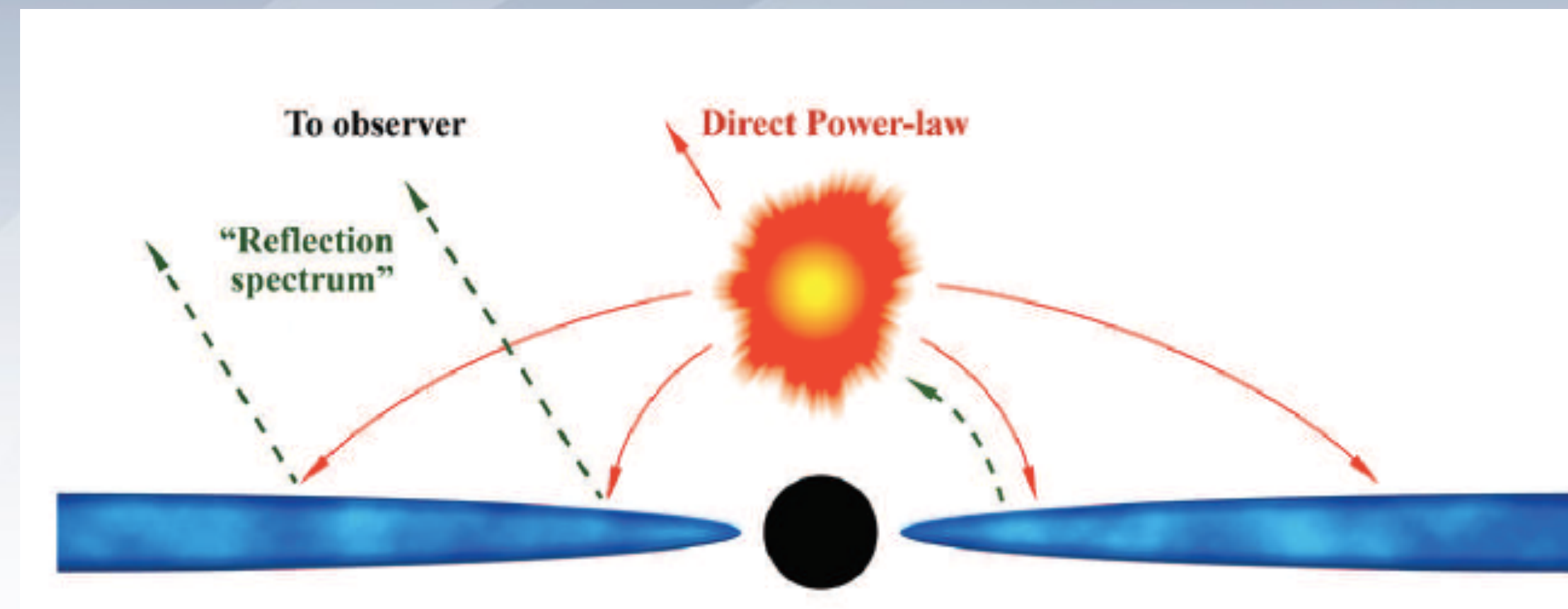
Scale sizes of Typical X-ray Sources

- Milli-arcsecond size
 - AGN jets
 - XRB jets, orbital scales
 - Stellar coronae
 - Gravitational Lenses
- Micro-arcsecond size
 - SMBH event horizons
 - AGN BLRs
 - Extragalactic SNRs
 - CV disks
 - XRB orbits
 - Pulsar light cylinders
 - Exoplanetary systems
 - Protoplanetary disks



Some Science Goals of a Micro-ArcSecond Imager

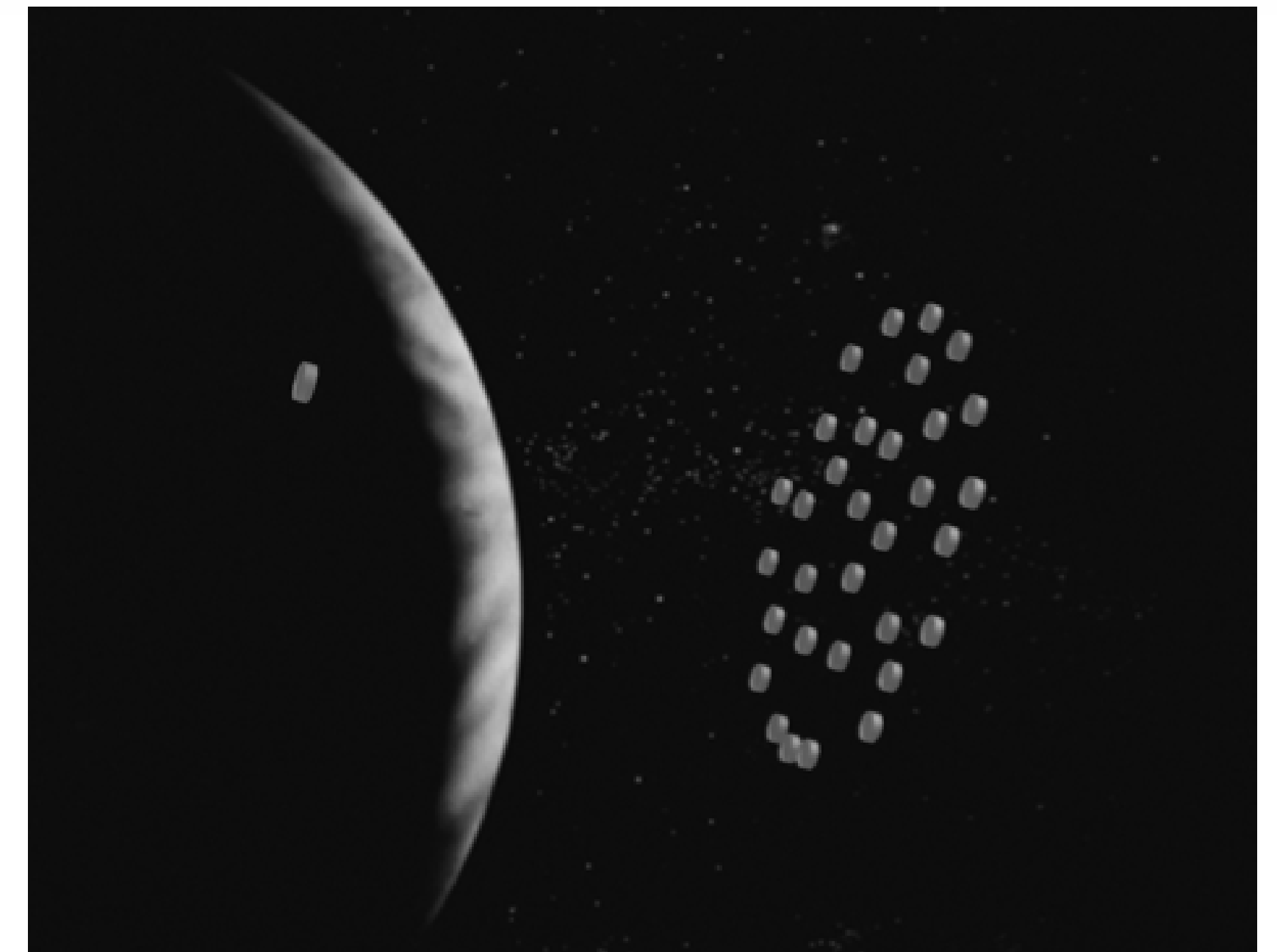
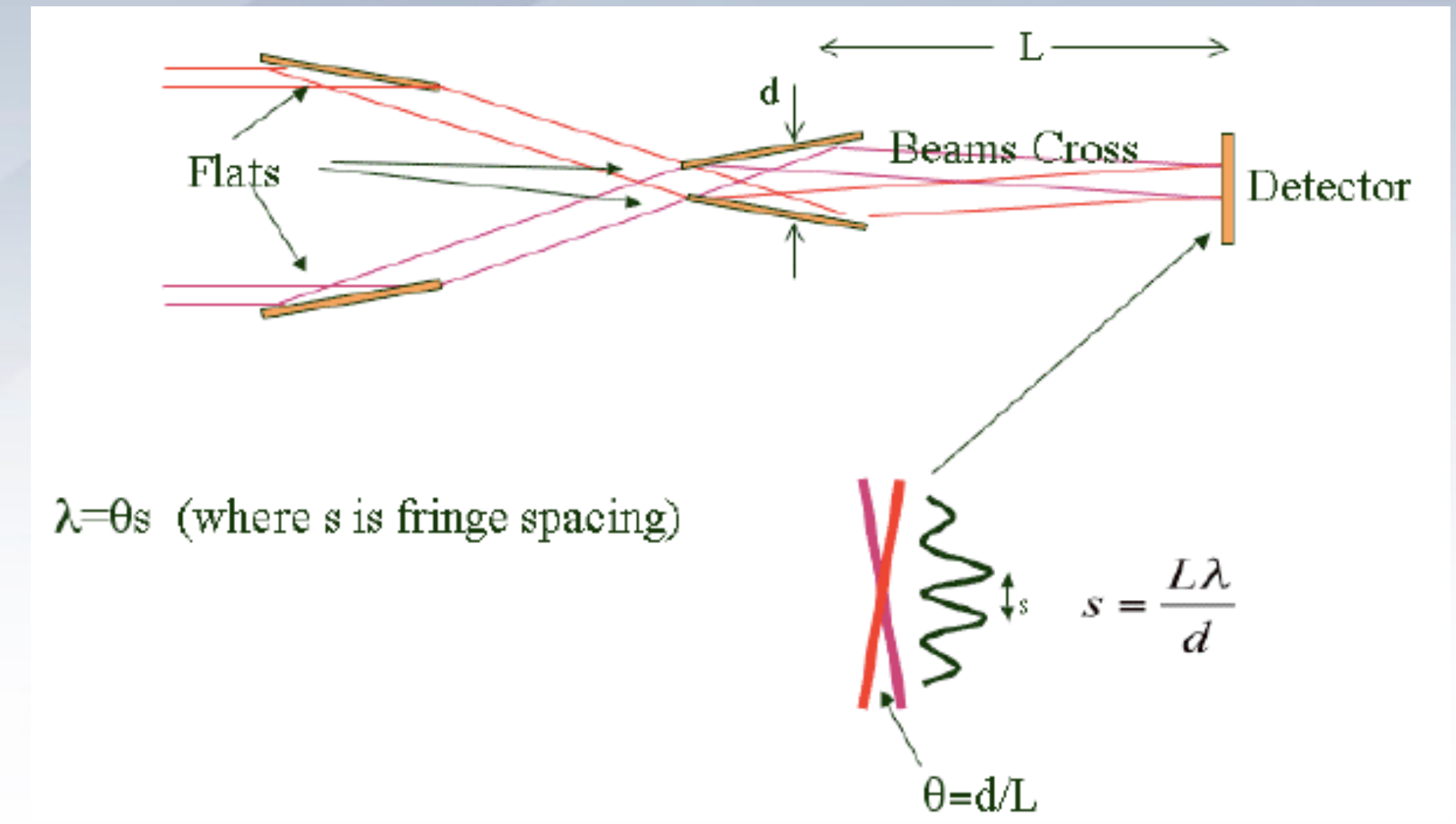
- Supermassive Black Holes in Active Galaxies
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 - Velocity mapping in Fe-K from reflection off disk
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- Measure GRB fireball expansion & jet speed
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- Resolve BH X-ray binaries to $< 10^7 \text{ km}$ at 10 kpc
 - Image accretion disk and separate irradiated companion
 - Image jets from SS 433, Cyg X-1, etc.
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- Stars
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 - Planetary systems, transiting exoplanets, star forming regions



η Carina

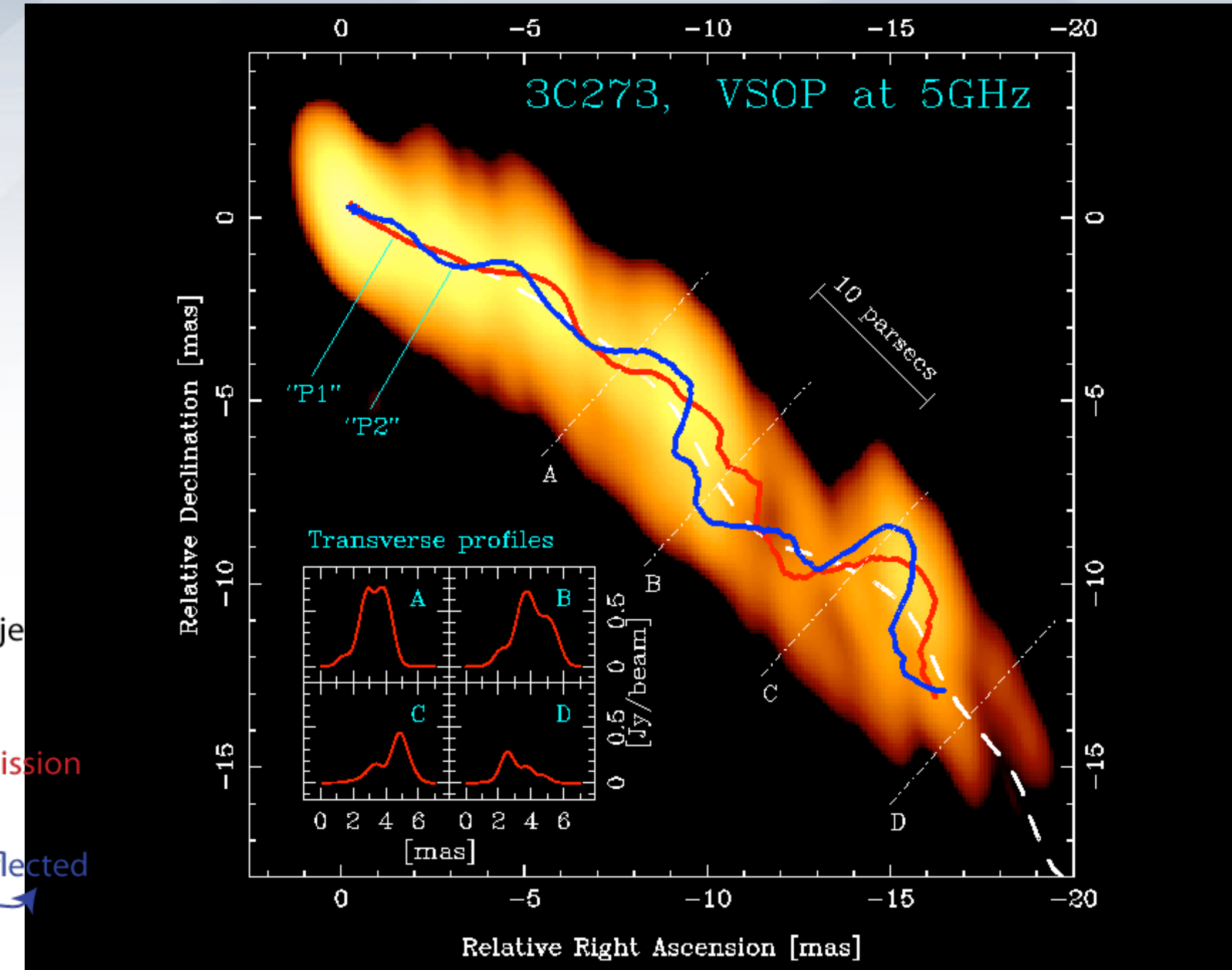
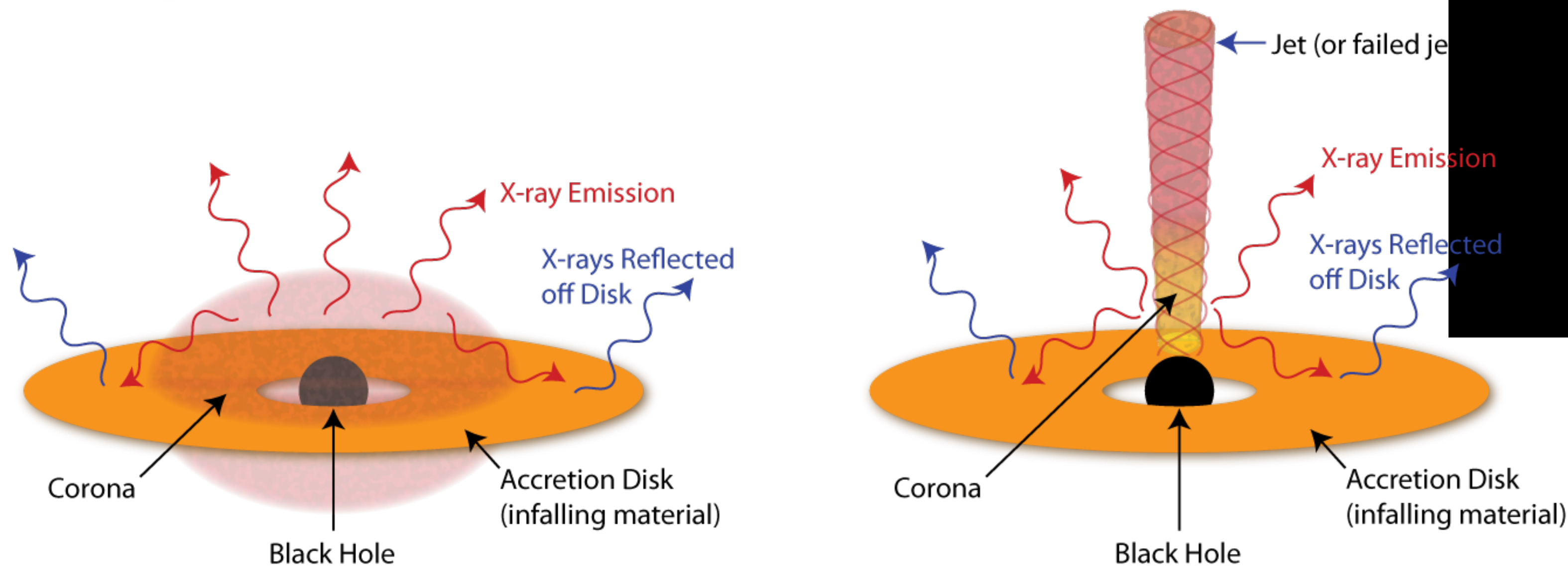
Previous Suggestions for Improving X-ray Imaging

- NASA Beyond Einstein “Vision Mission”: a black hole imager
 - Science goal: image BHs in nearby AGN
 - Instrument goal: 0.000,000,1” angular resolution
 - MAXIM: X-ray interferometry with 100+ m baseline
 - Pathfinder: 0.000,1” resolution, 0.14 m primary size, 2 spacecraft 450 m apart
- One alternative: normal incidence telescope with multilayer (ML) coatings
 - Proposed by Windt and Kahn (2003)
 - Tune MLs to lines of ions in 17-35Å range
 - Distribute 2.5m mirrors over 50m aperture
 - Pathfinder: 0.000,3”, 2.5 m diam primary, Cassegrain design, 10 m focal length
- Another alternative: combine diffractive & refractive optics
 - See Skinner (2001, 2002), Gorenstein (2007)
 - Good option for γ -ray imaging



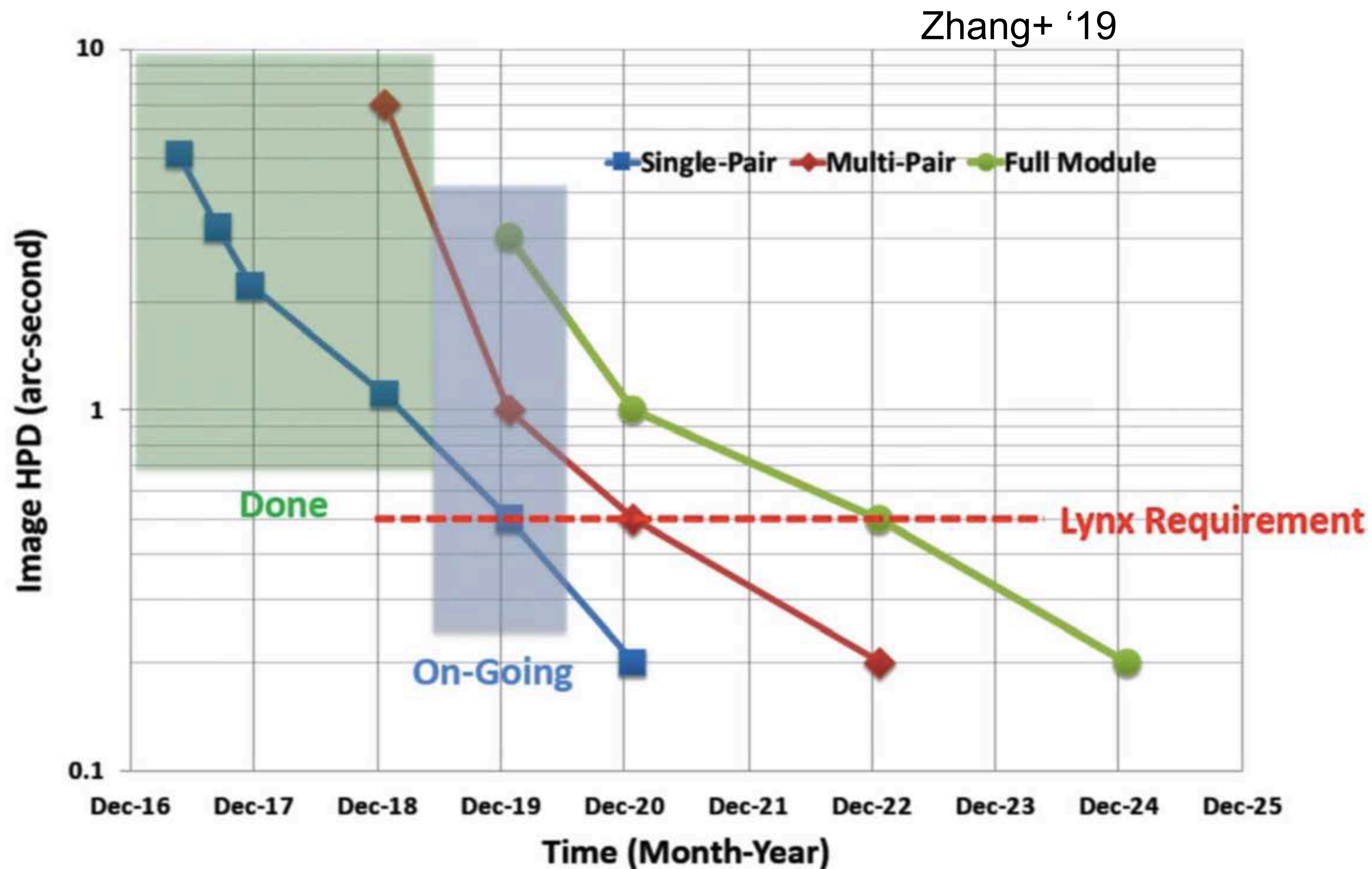
Imaging AGN Cores: 3C 273

- Discern between jet and coronal models
- VLBI shows core is a jet about 25 mas long
- Core flux is 0.15 ph/cm²/s/keV at 0.4 keV
- Requires imaging < 0.01"
- A ML-based mirror can get 100 cnt/PSF in 10⁵ s



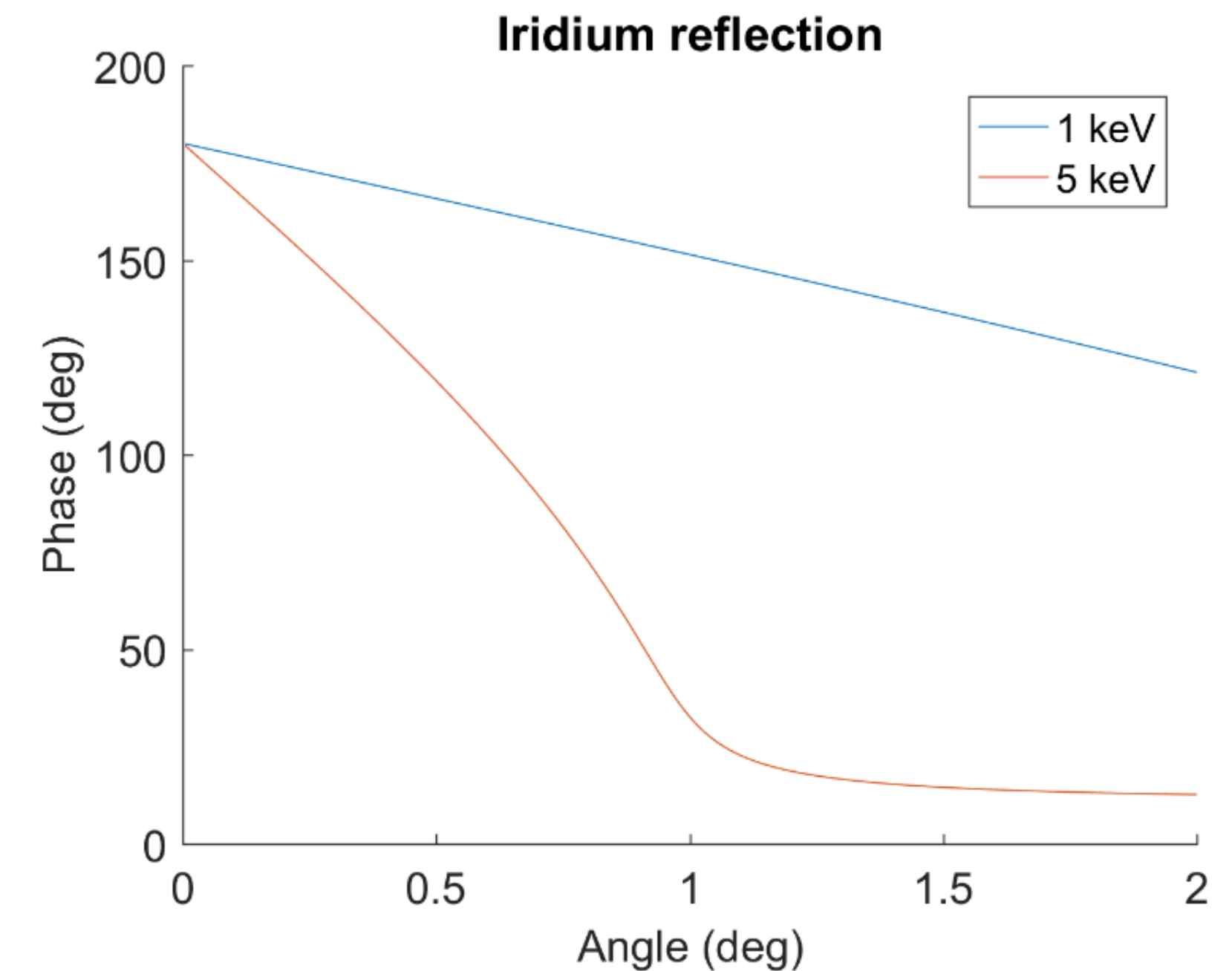
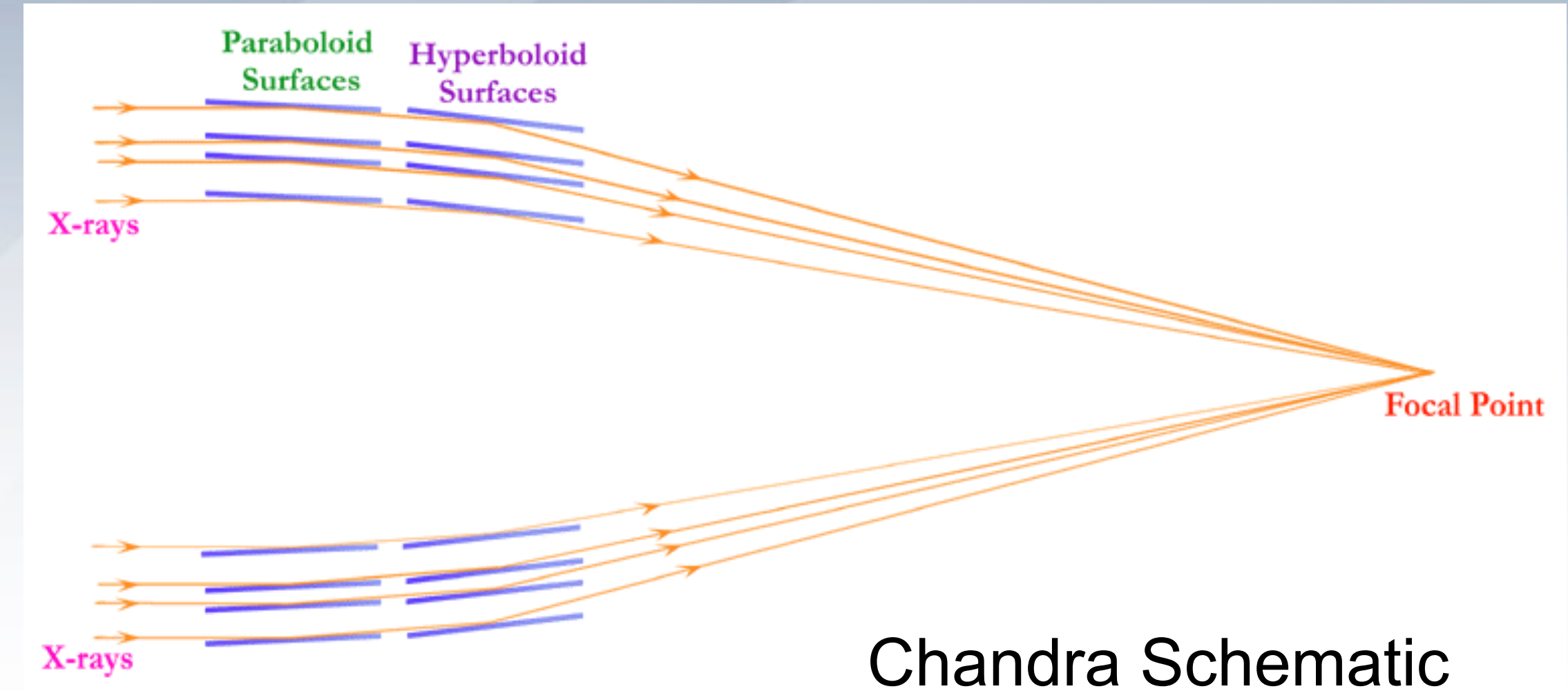
Diffraction Limited Si Mirrors

- Now near diffraction limit per mirror at grazing incidence
- $\delta\theta = \lambda/D = \lambda/(L \sin \alpha)$
 - α = graze angle (0.2-0.5°)
 - L = mirror length (0.1 m)
 - $\delta\theta = 0.4\text{-}0.9''$ @ 1 keV
 - $\delta\theta = 0.1\text{-}0.2''$ @ 5 keV
- Development timetable achieves diffraction limit for mirror modules



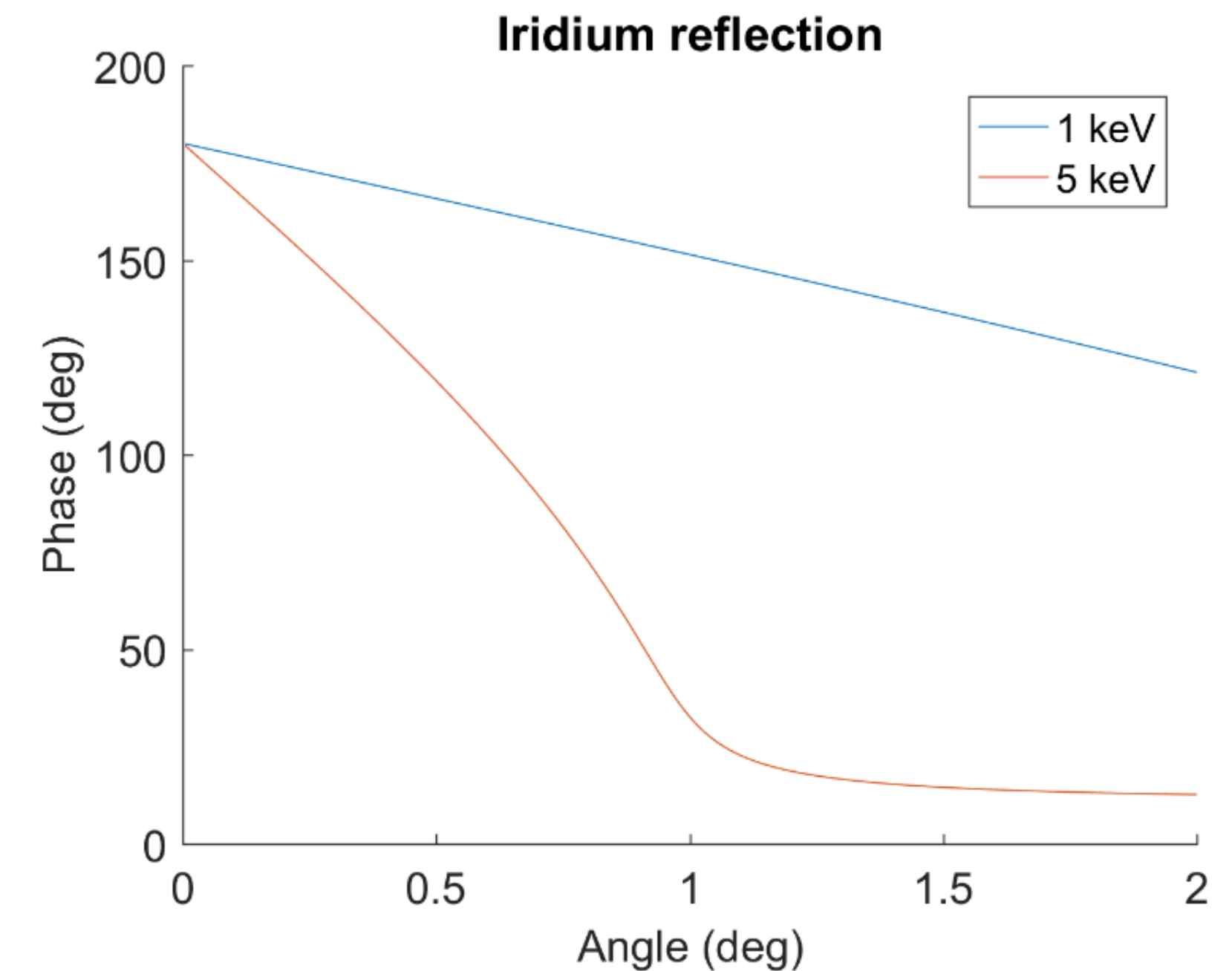
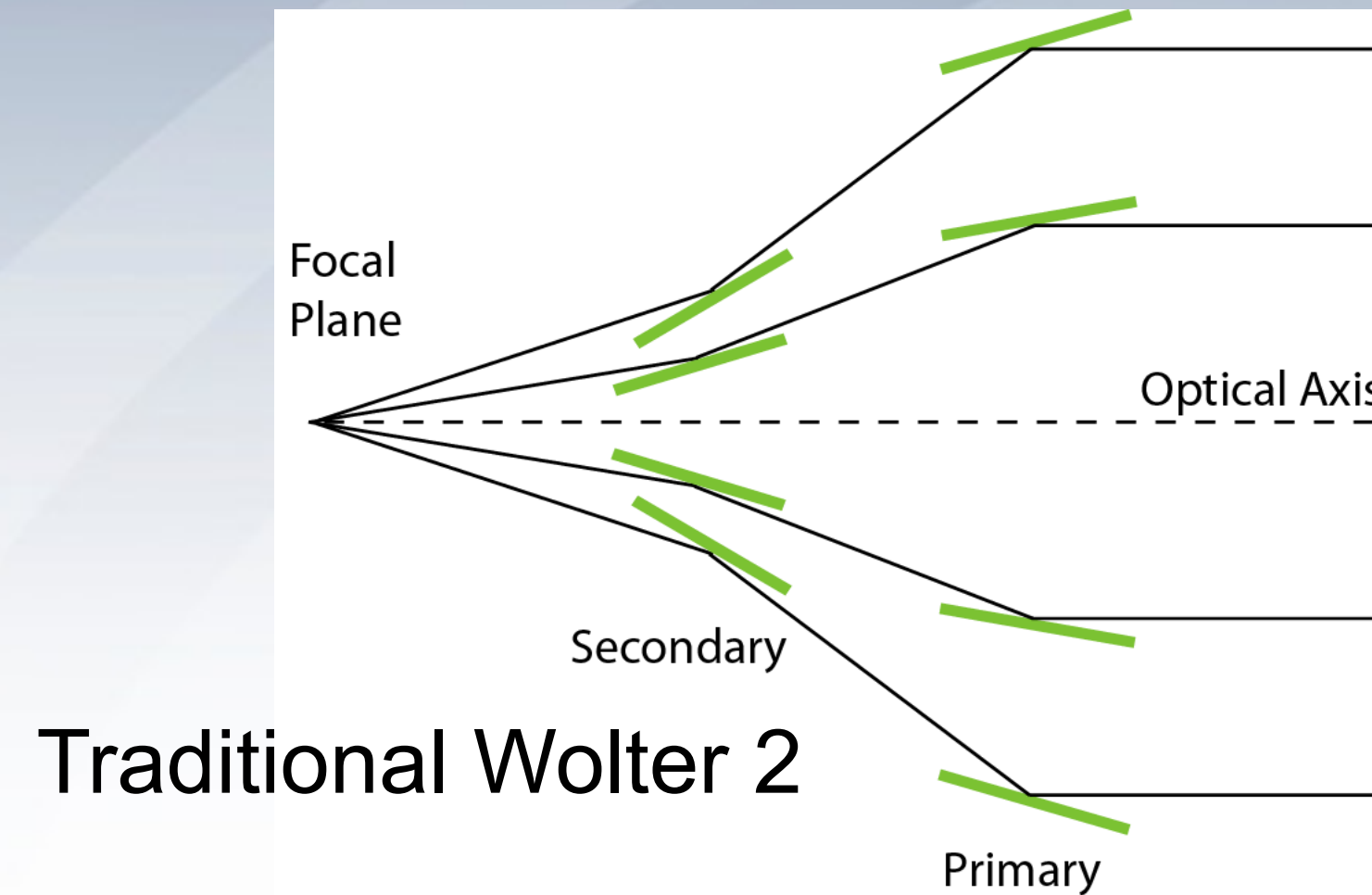
AAA Optical Design for Grazing Incidence Optics

- Aplanatic Wolter type 2
 - Obeys Abbe sine rule: constant magnification
 - Eliminates 1st order spherical or coma aberration
- Achronat
 - Obeys Fermat's principle: all rays have the same optical path length (OPL) to focus
 - Wolter I assemblies have large OPL differences (Chandra: $>10\text{ mm} \gg \lambda$)
 - Fermat's principle is constraint of new design
- Achromat
 - Indices of refraction are $f(E)$: photon phase depends on graze angle across aperture
 - WS I telescopes are not phase coherent
 - Achromaticity verified numerically a posteriori

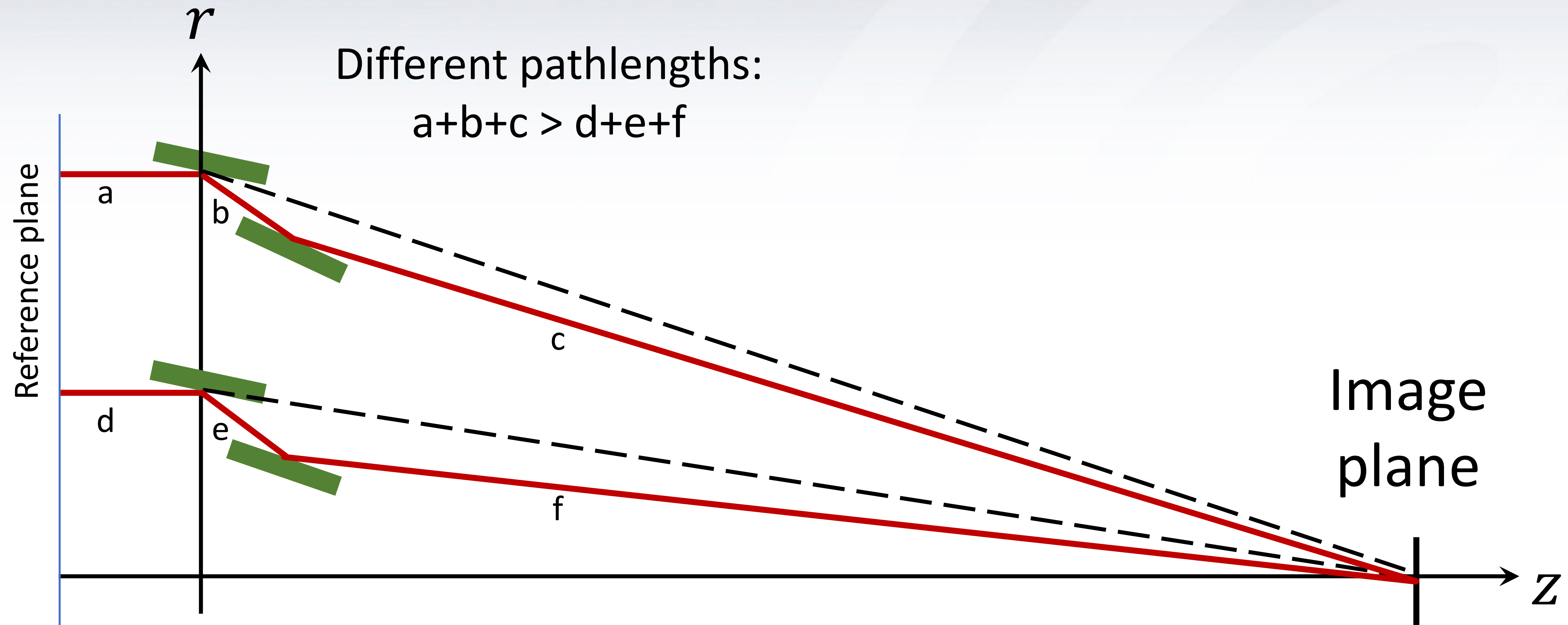


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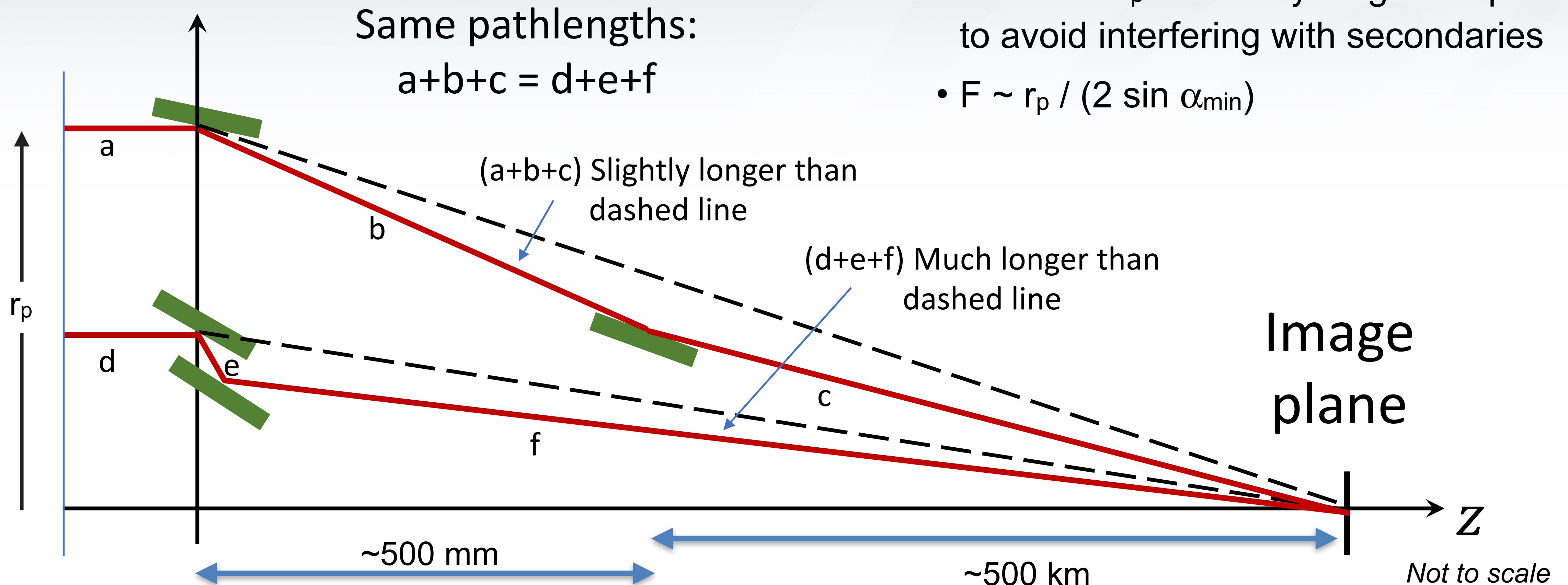


How to Fix Grazing Incidence Optics for Interferometry



Schematic of a Design for Grazing Incidence Interferometry

- Graze angle α decreases with r_p
- Secondary farther from aperture with r_p
- Minimum r_p limited by lengths of primaries to avoid interfering with secondaries
- $F \sim r_p / (2 \sin \alpha_{\min})$

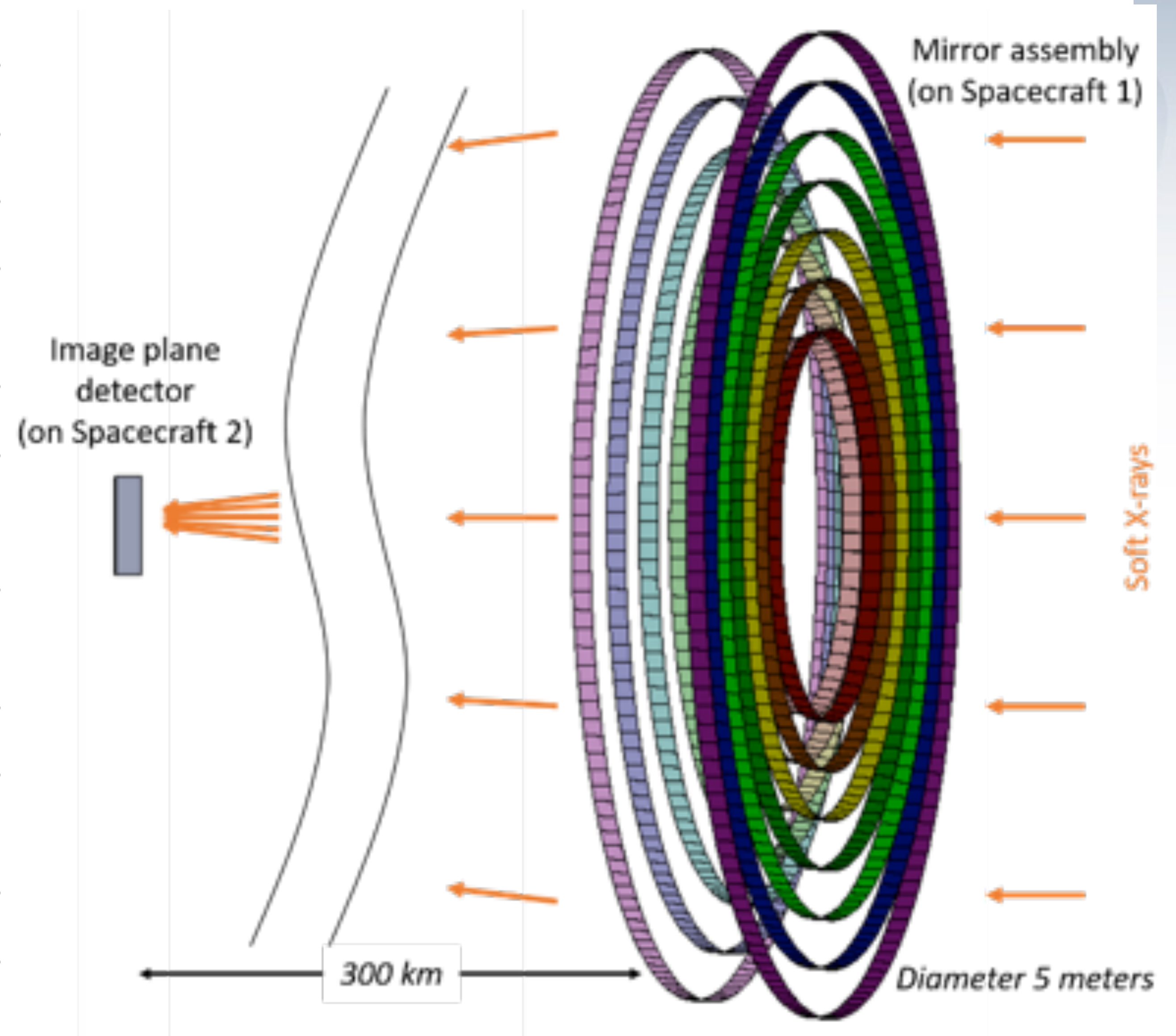


Sample Design

Fixed $L = L^*$, variable $h_0 - h_2, z_2, i_0$

Focal length	500 km
Shell radii	1.25 m to 2.50 m
Graze angles	0.50° to 0.17°
Mirror size	100 mm long, 1 mm thick
Reflective coating	Iridium ($5 \text{ \AA}$ roughness)

PSF	$17 \text{ } \mu\text{s HPD @ 5 keV}$ ($40 \text{ } \mu\text{m}$ at image plane)
Effective area	$2.77 \text{ m}^2 \text{ @ 5 keV}$
Total mirror surface area	1500 m^2 ($\sim 4\text{x Lynx}$)
Total mirror mass	3500 kg ($\sim 8\text{x Lynx}$)



Sample Design

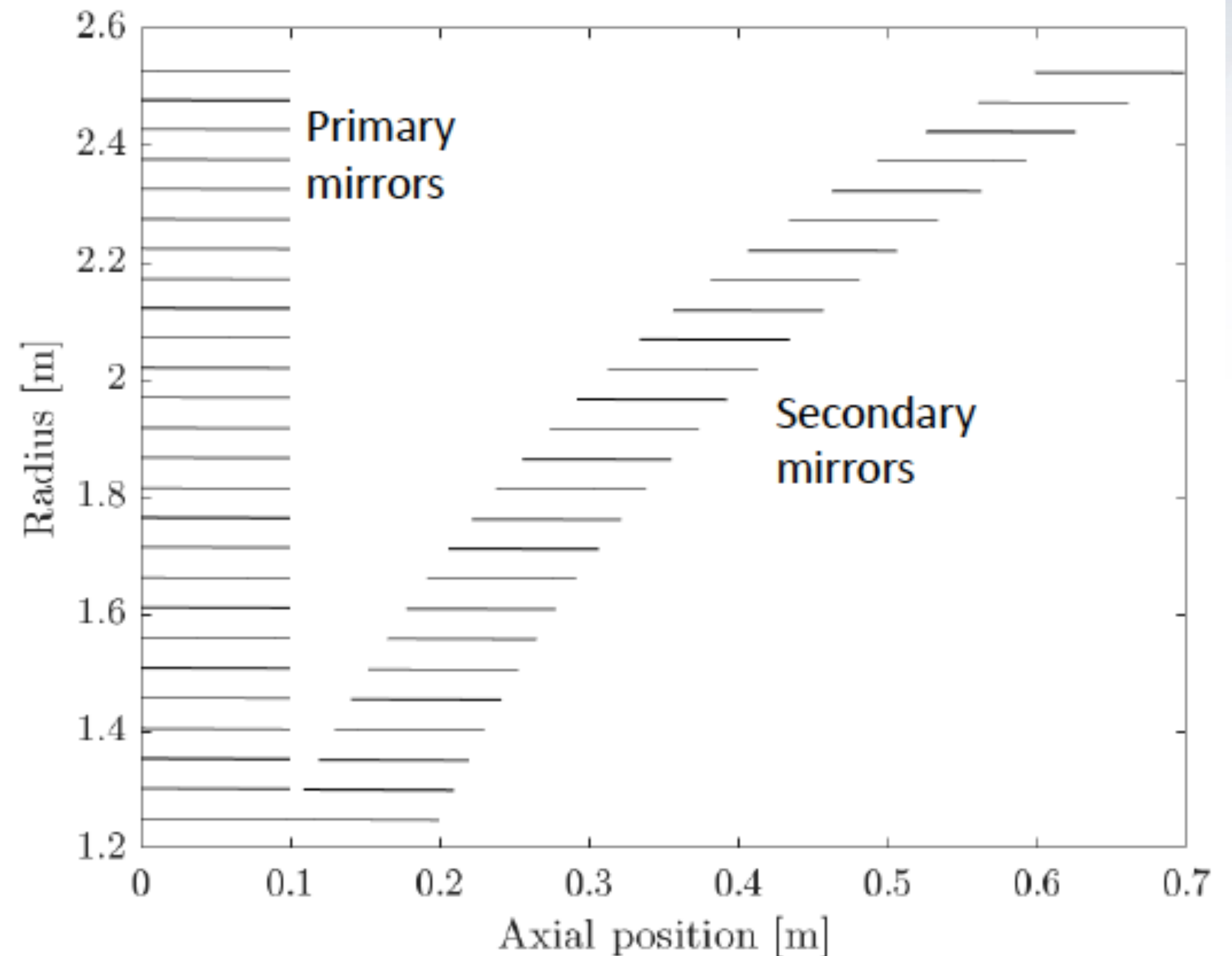
Fixed $L = L^*$, variable $h_0 - h_2, z_2, i_0$

Focal length	500 km
Shell radii	1.25 m to 2.50 m
Graze angles	0.50° to 0.17°
Mirror size	100 mm long, 1 mm thick
Reflective coating	Iridium (5 Å roughness)

PSF	17 μ as HPD @ 5 keV (40 μ m at image plane)
Effective area	2.77 m ² @ 5 keV
Total mirror surface area	1500 m ² (~4x Lynx)
Total mirror mass	3500 kg (~8x Lynx)

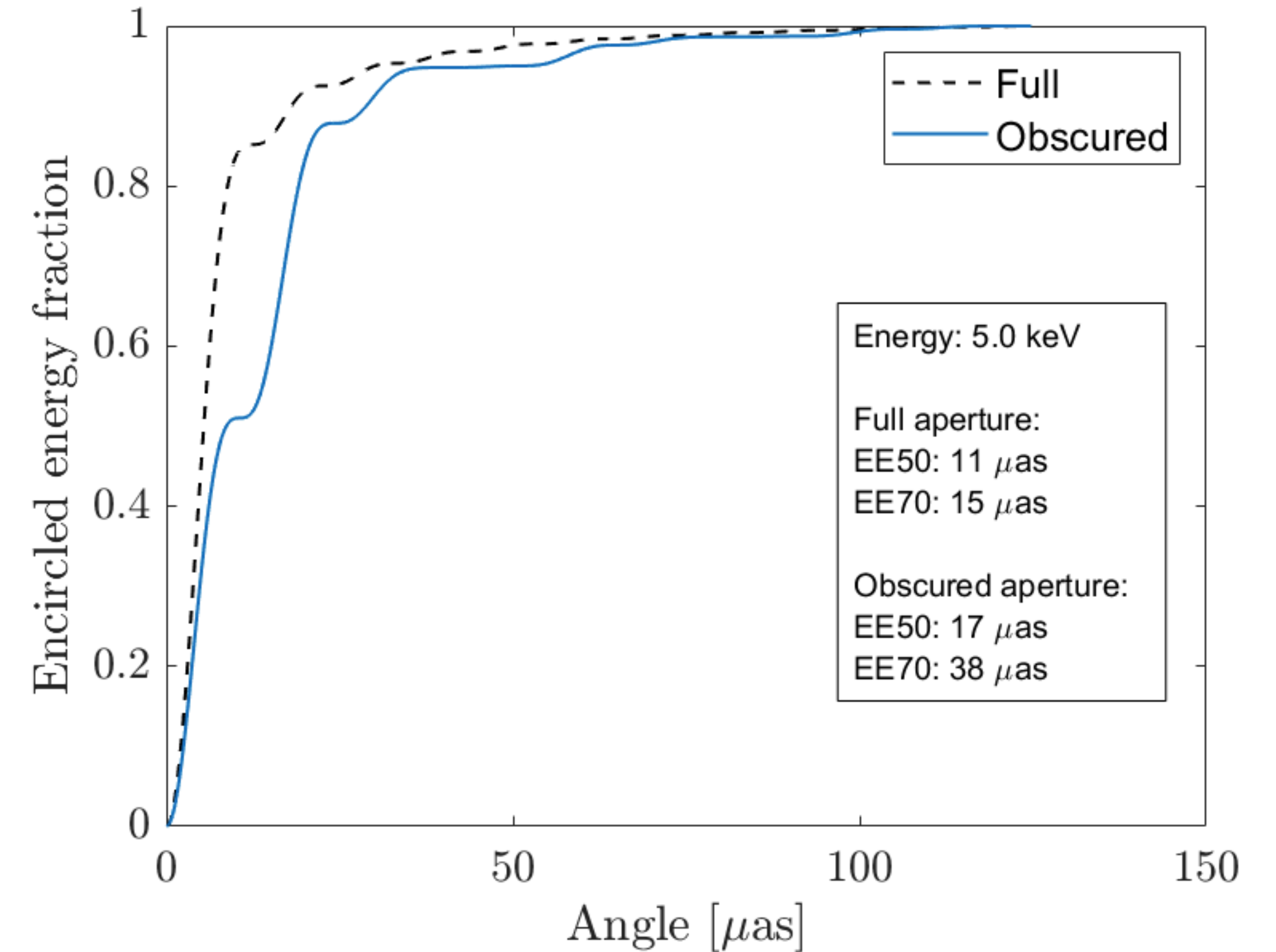
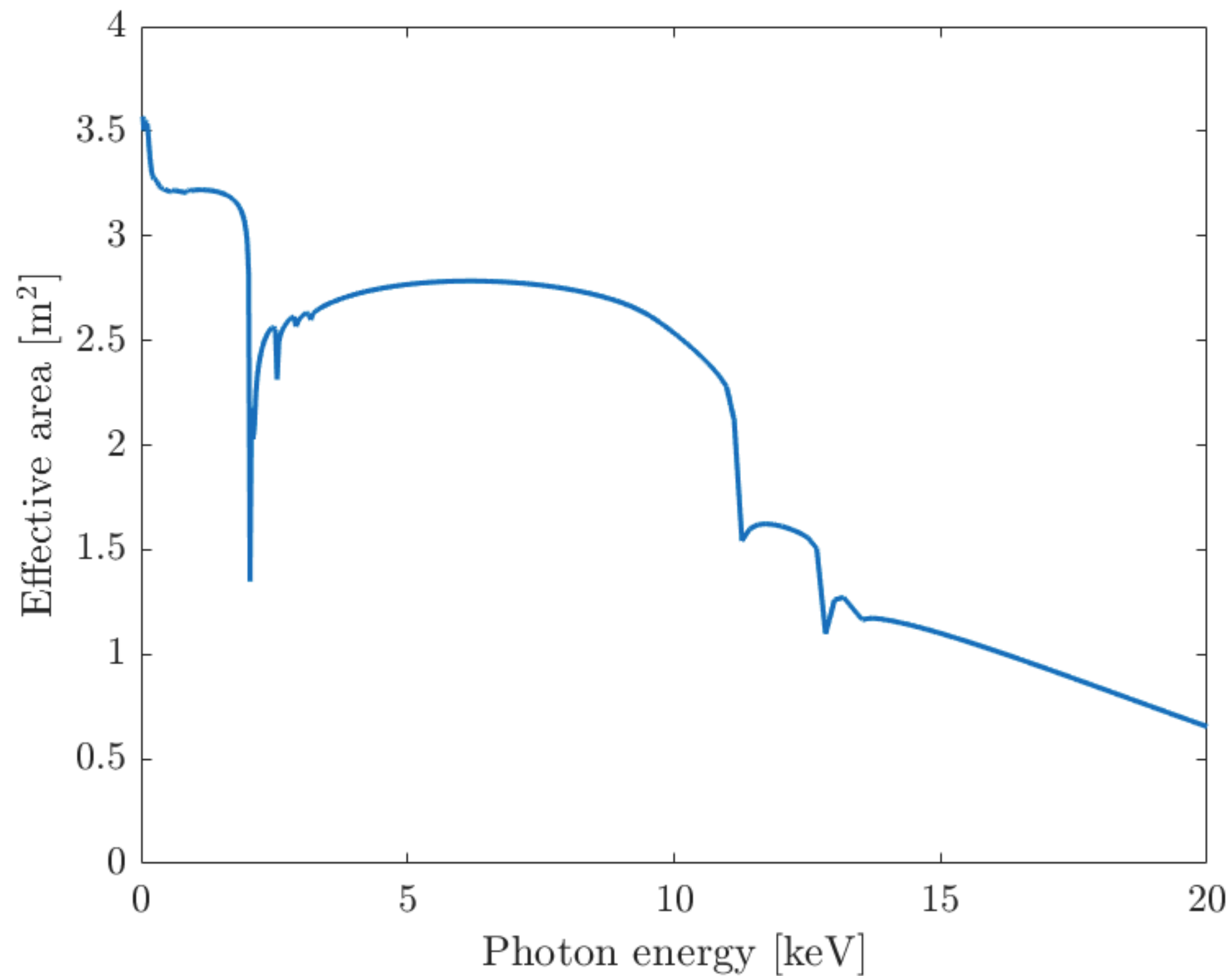
Mirror assembly layout

Low-density aperture fill shown for illustration clarity



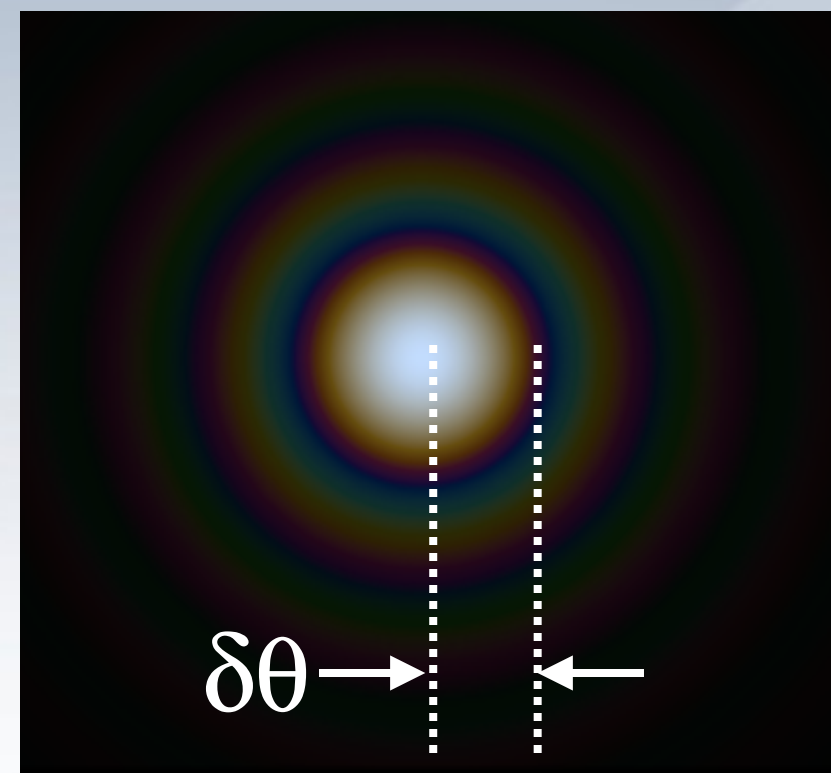
Sample Telescope Performance

- Effective area at high E increases with shell diameter
- Obscuration (by shell thicknesses) & unfilled aperture increases HPD



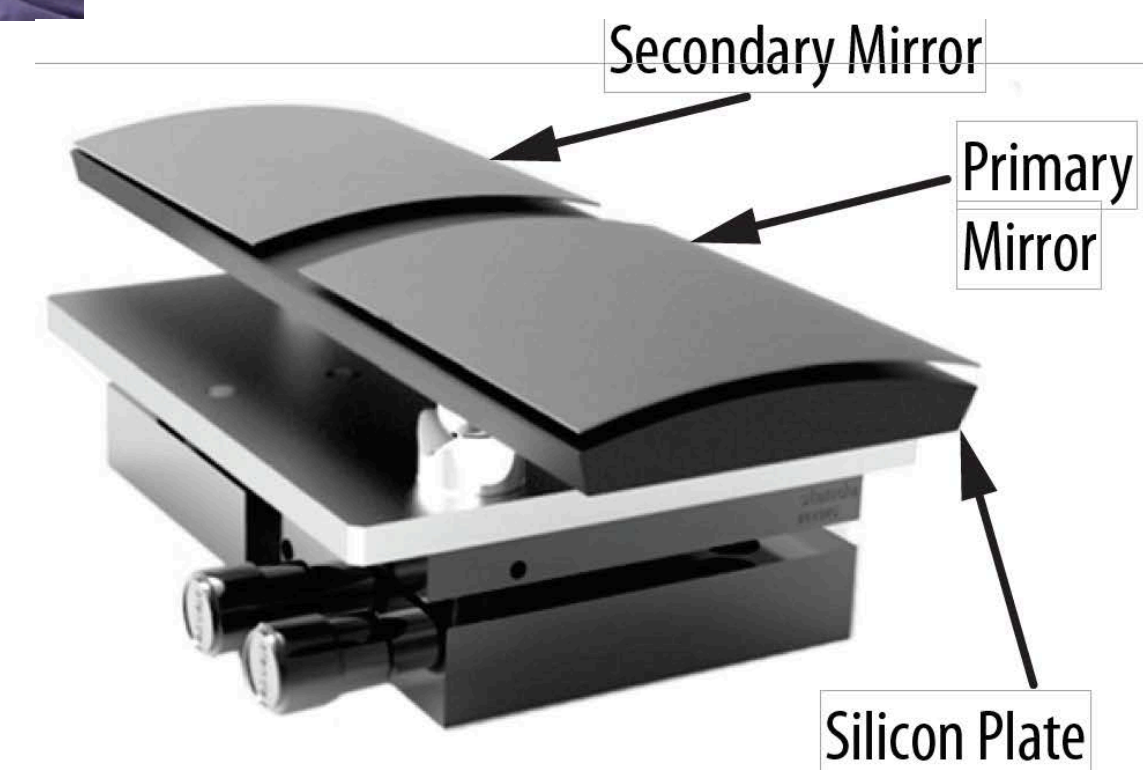
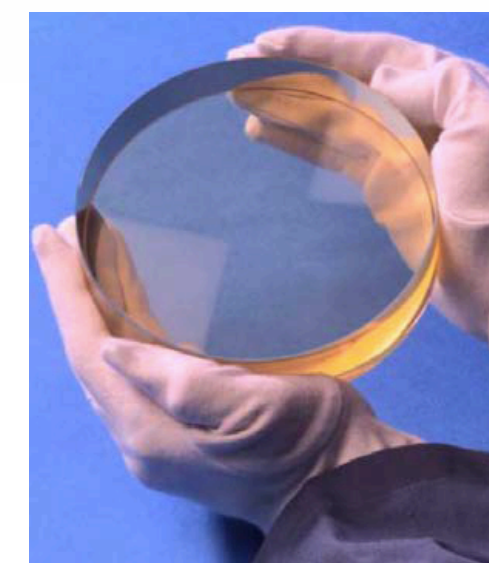
Resolution Drives Aperture Size Pixel Size Drives Telescope Length

- Imaging resolution ($\delta\theta$, Rayleigh criterion)
 - $\delta\theta = 1.22 \lambda/D = 0.25 \text{ mas } (\lambda/\text{nm}) / (D/\text{m})$
 - $2 \text{ mas @ } 3 \text{ nm} \Rightarrow D = 0.4 \text{ m}$
 - $0.1 \mu\text{as @ } 0.1 \text{ nm} \Rightarrow D = 250 \text{ m}$



White light Airy disk

- Effective focal length (F)
 - $F = \delta x / \delta\theta = 410 \text{ m } (\delta x/\mu) / (\delta\theta/\text{mas})$
 - $50 \text{ mas, } 5 \text{ nm, } \delta x = 3 \mu \Rightarrow F = 25 \text{ m}$
 - $2 \text{ mas, } 3 \text{ nm, } \delta x = 2 \mu \Rightarrow F = 410 \text{ m}$ } Normal Incidence
 - $0.1 \text{ mas @ } 1 \text{ nm, } \delta x = 1 \mu \Rightarrow F = 4.1 \text{ km}$
 - $0.1 \text{ mas @ } 0.1 \text{ nm, } \delta x = 0.2 \mu \Rightarrow F = 820 \text{ km}$ } Grazing Incidence



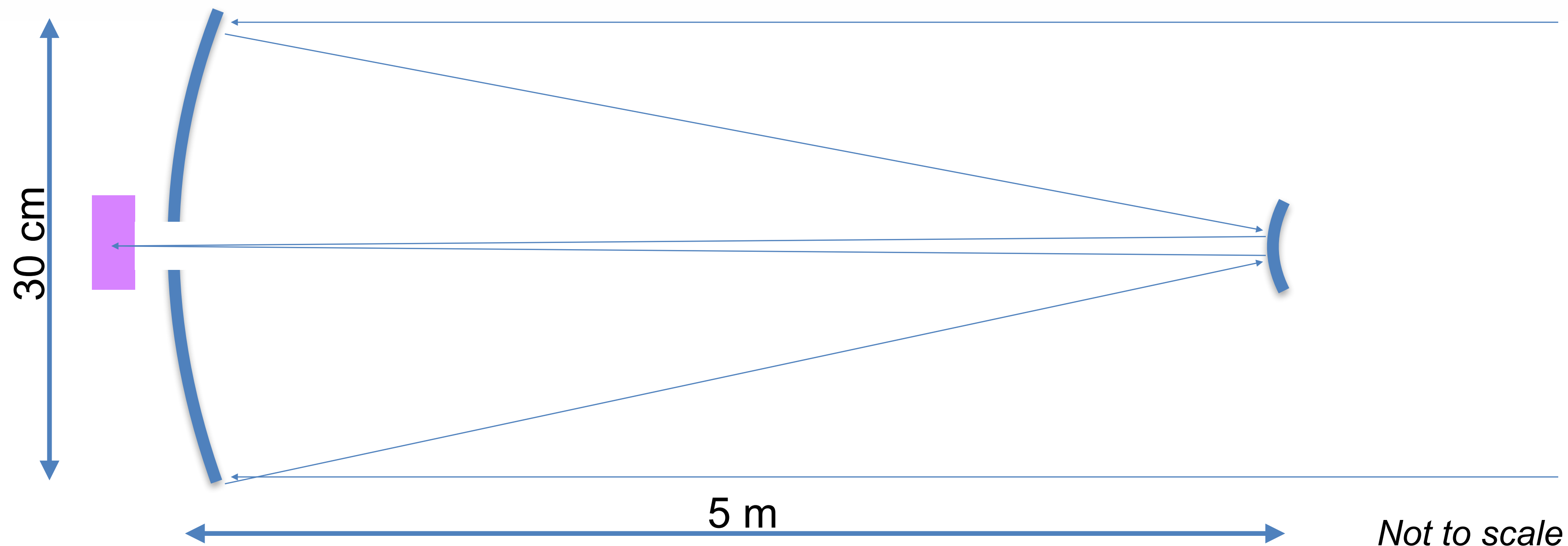
Zhang+ '19

A Near-Term Option: Normal Incidence Milliarcsecond X-ray Imager

- **Approach:** Normal Incidence Multilayer optics
- Diffraction-limited mirror at 0.25-0.40 keV (3-5 nm)
- ML coatings give 10-20% reflectivity, 2% band
- 1-2 μ localization drives 100 m effective focal length
- Cassegrain optical design for 2 mas
- **Technologies:** Mirror figure to 0.05 nm and ML coatings, high resolution X-ray detectors, structure stability, mirror verification at X-rays, attitude knowledge

Timetable:

- **Stage 1 (5 yr):** imaging to 50 mas
- **Stage 2 (10 yr):** imaging to 2 mas
- **Long-term:** finder scope for micro-arcsecond imager?
- **Science:** Quasar & XRB jet imaging, astrometry to 10 microarcsecond, resolving binaries, planets, etc.



Steps to a Black Hole Imager

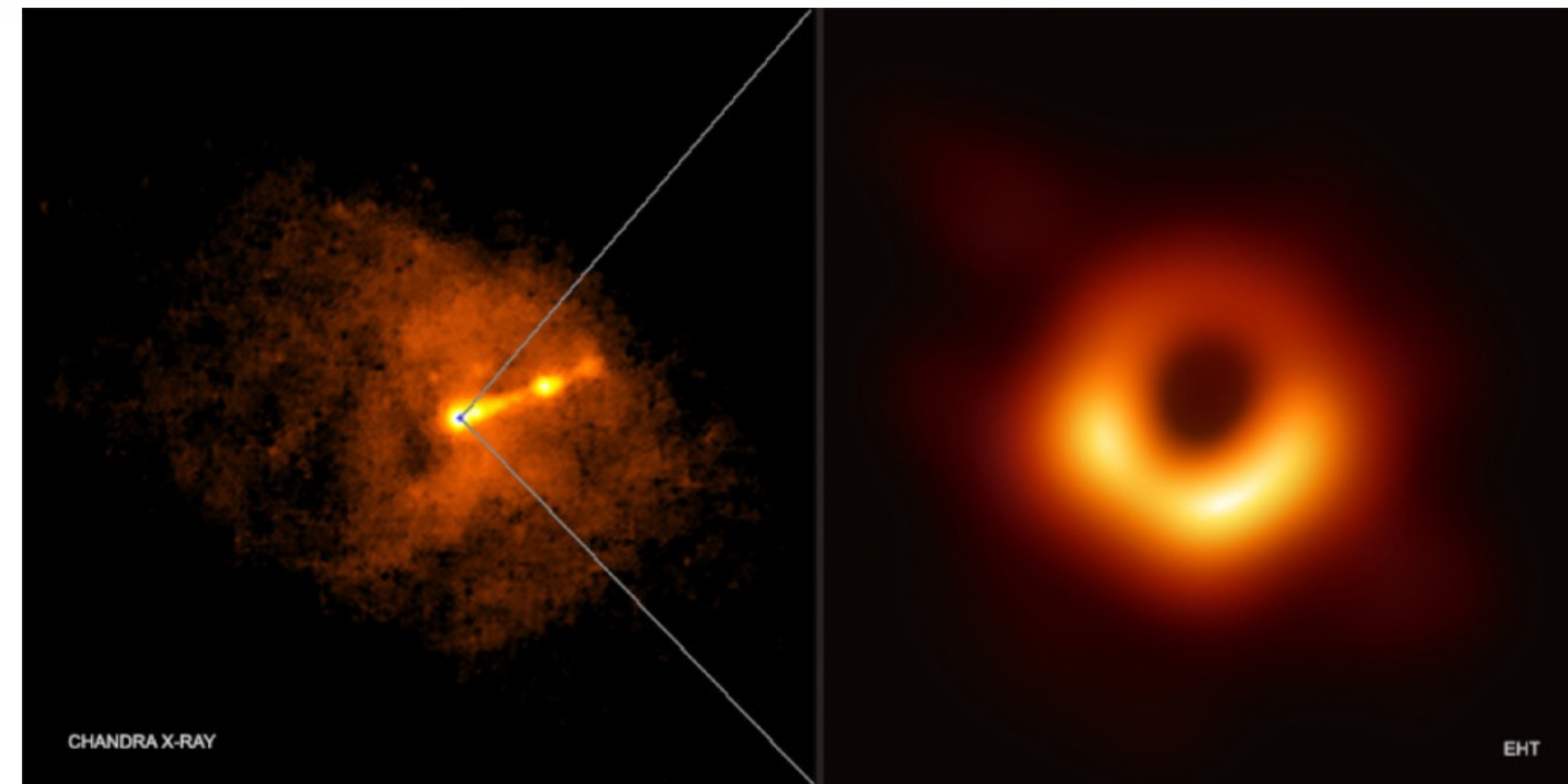
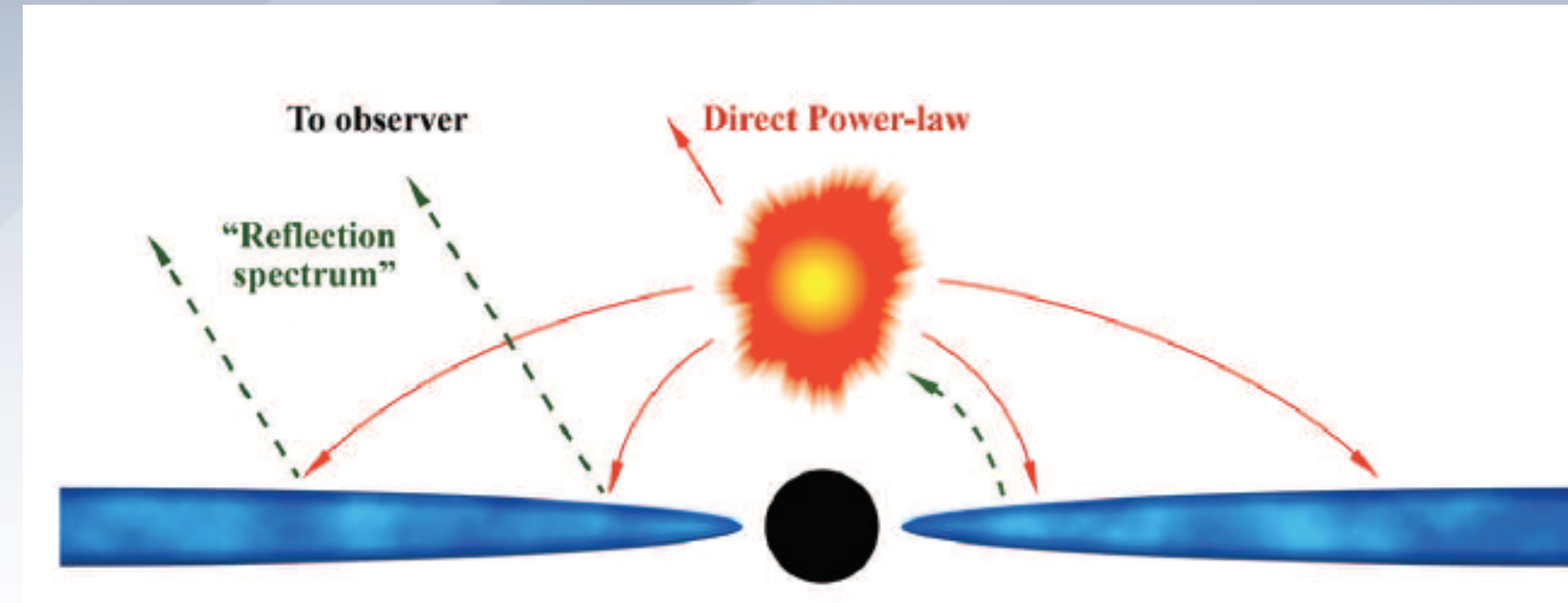


- 0.05" in a ML-based SmallSat
 - 10 mas knowledge
 - small pixel detectors
- 0.002" in a ML-based SMEX
 - sub-mas knowledge
 - folded beam, active secondary
 - X-ray ref. frame
- 0.0001" in a grazing-incidence Probe (single s/c mirror)
 - μ " knowledge
 - formation flying detector
 - ground X-ray testing
- 0.000,003" grazing-incidence Flagship
 - mirrors in formation flying
 - sub- μ " knowledge
- 0.000,000,1" grazing-incidence Black Hole Imager

- Science team
 - Set long-term and intermediate objectives
 - Establish priorities
 - Foster theory
 - Event horizon accretion
 - Relativistic jets
 - Accretion disk outflows
 - Stellar flare effects on planets
 - Explore!
- Engineering development timetable
 - Attitude knowledge, reference frame
 - Metrology and dynamic structures
 - Formation flying
 - Several detector spacecraft?
 - Add optics to expand u-v coverage and area

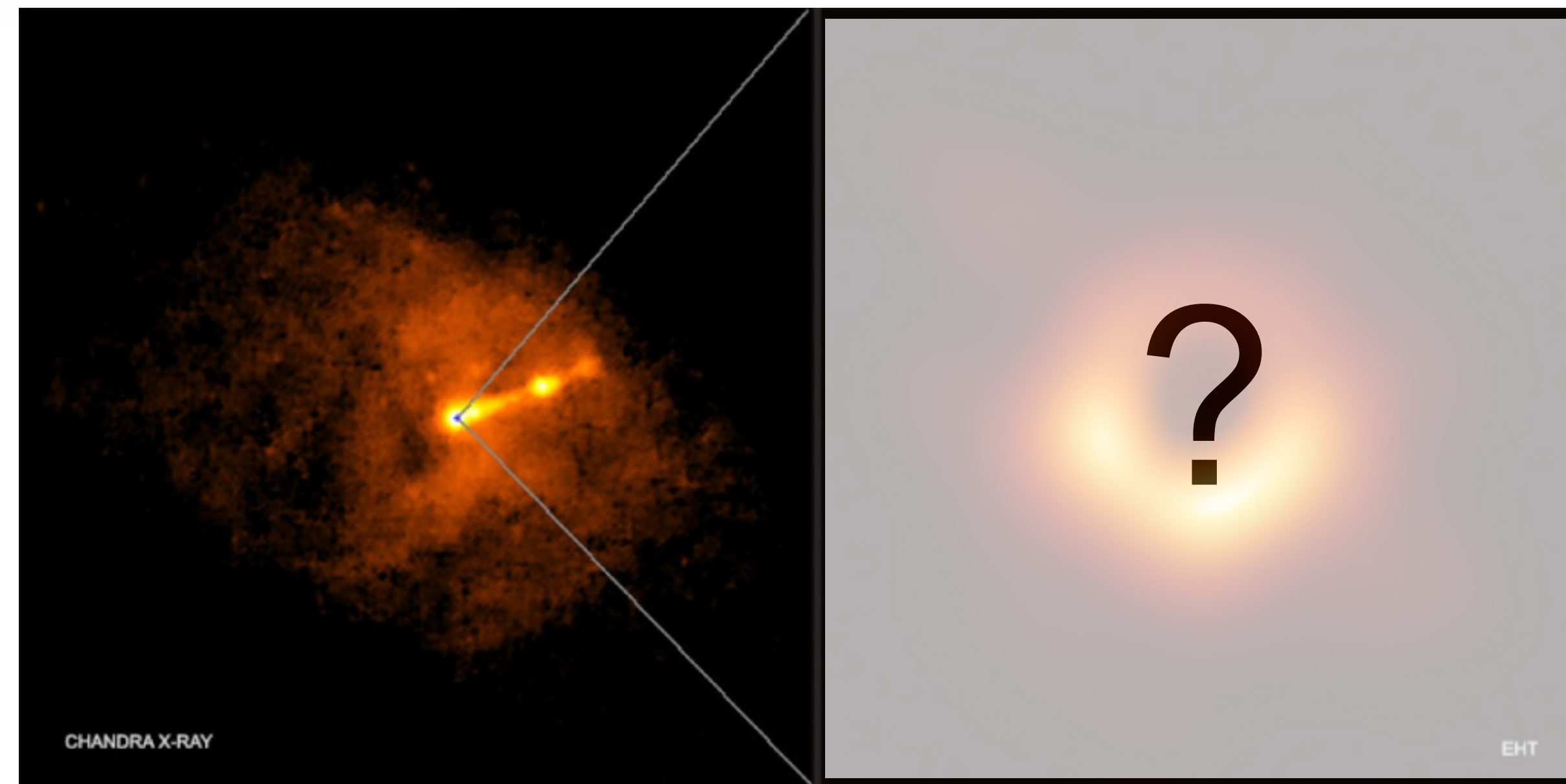
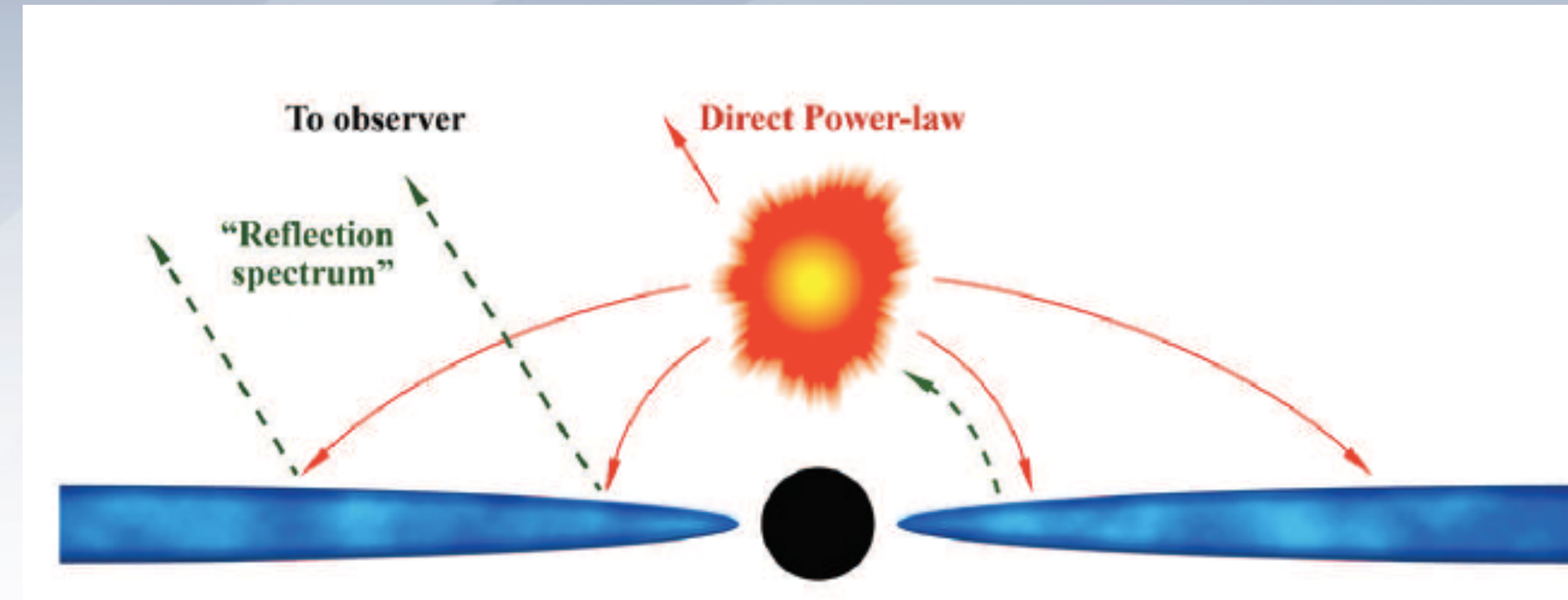
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Backup Slides

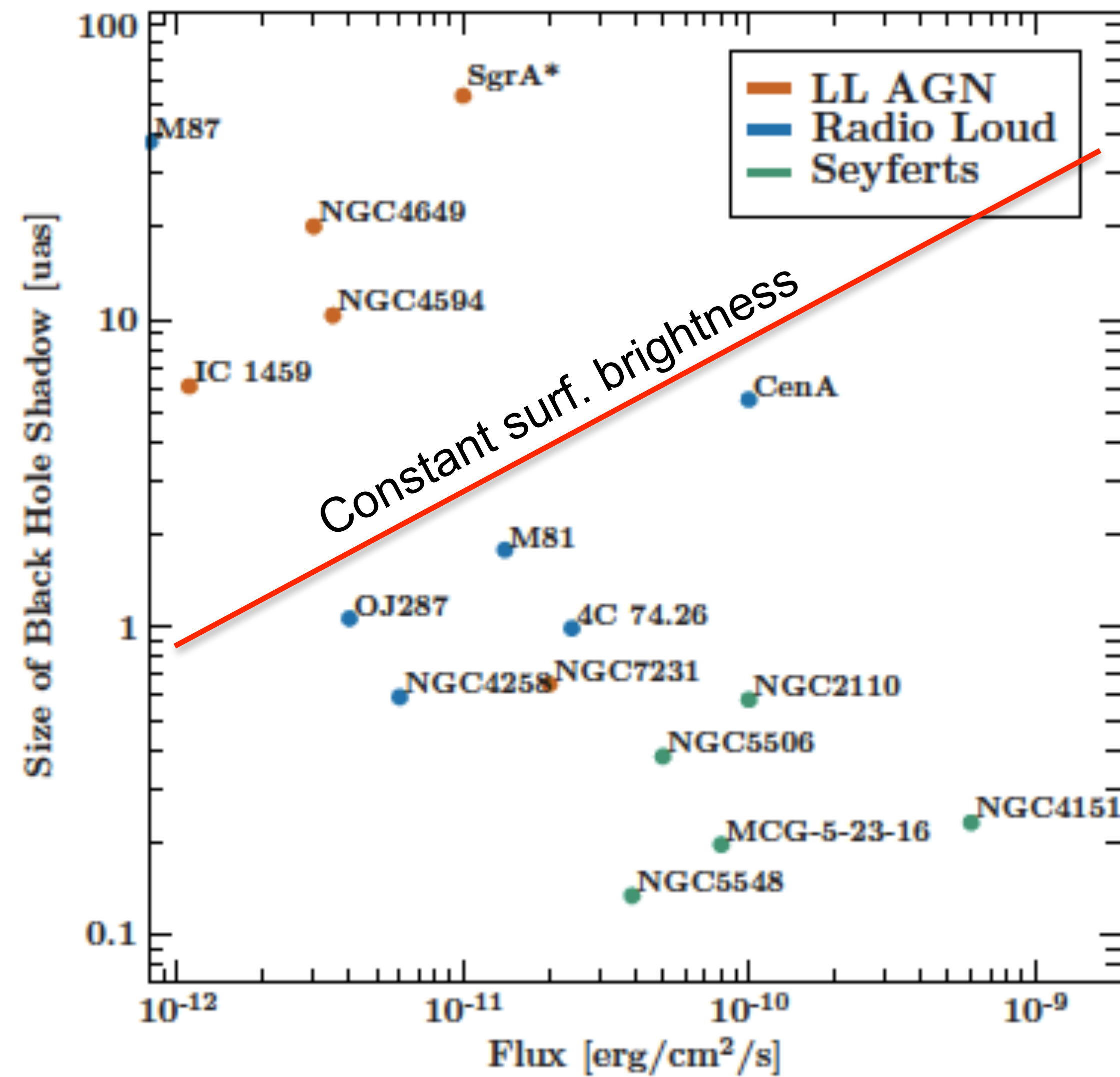
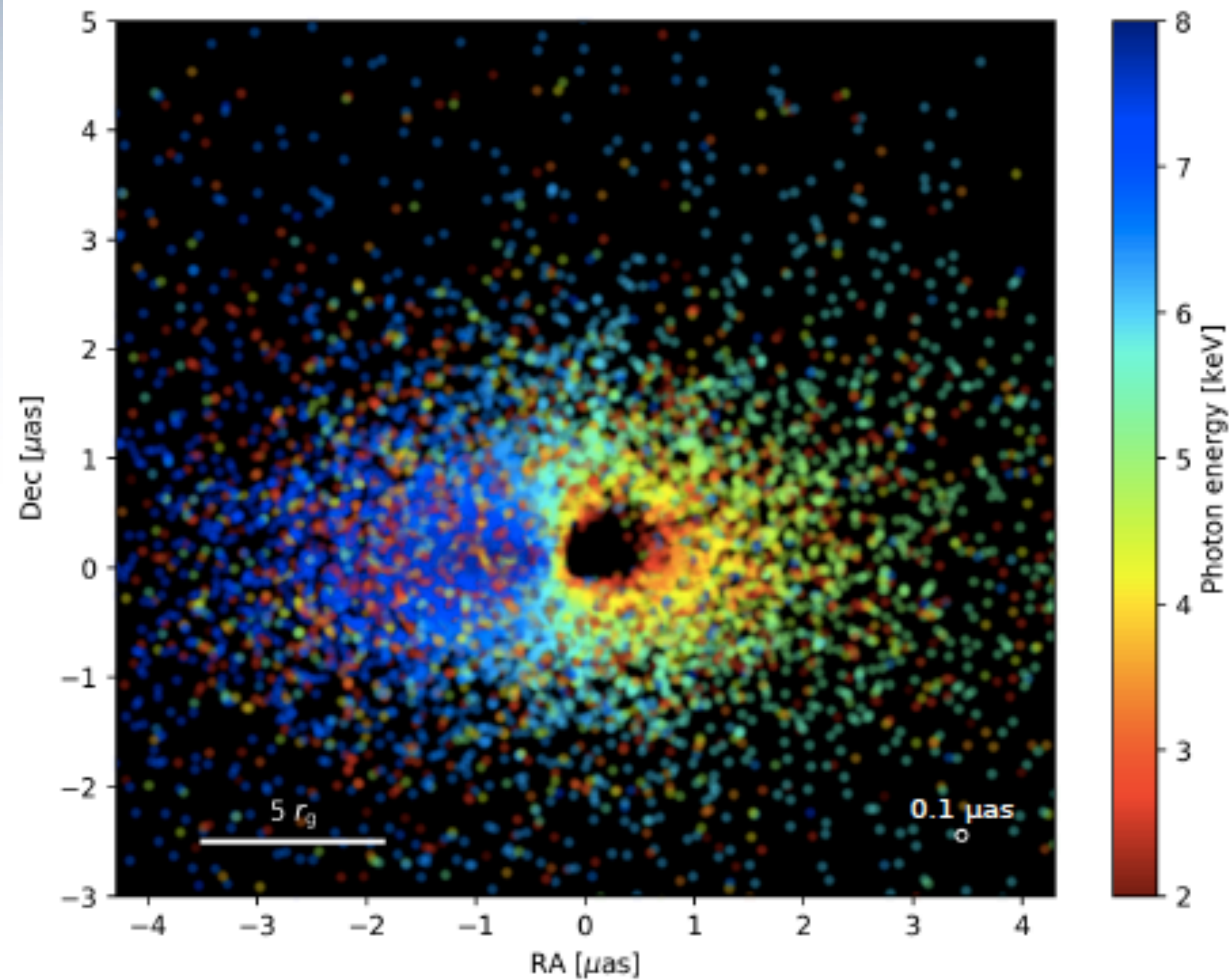


Prospects for Normal Incidence Imaging



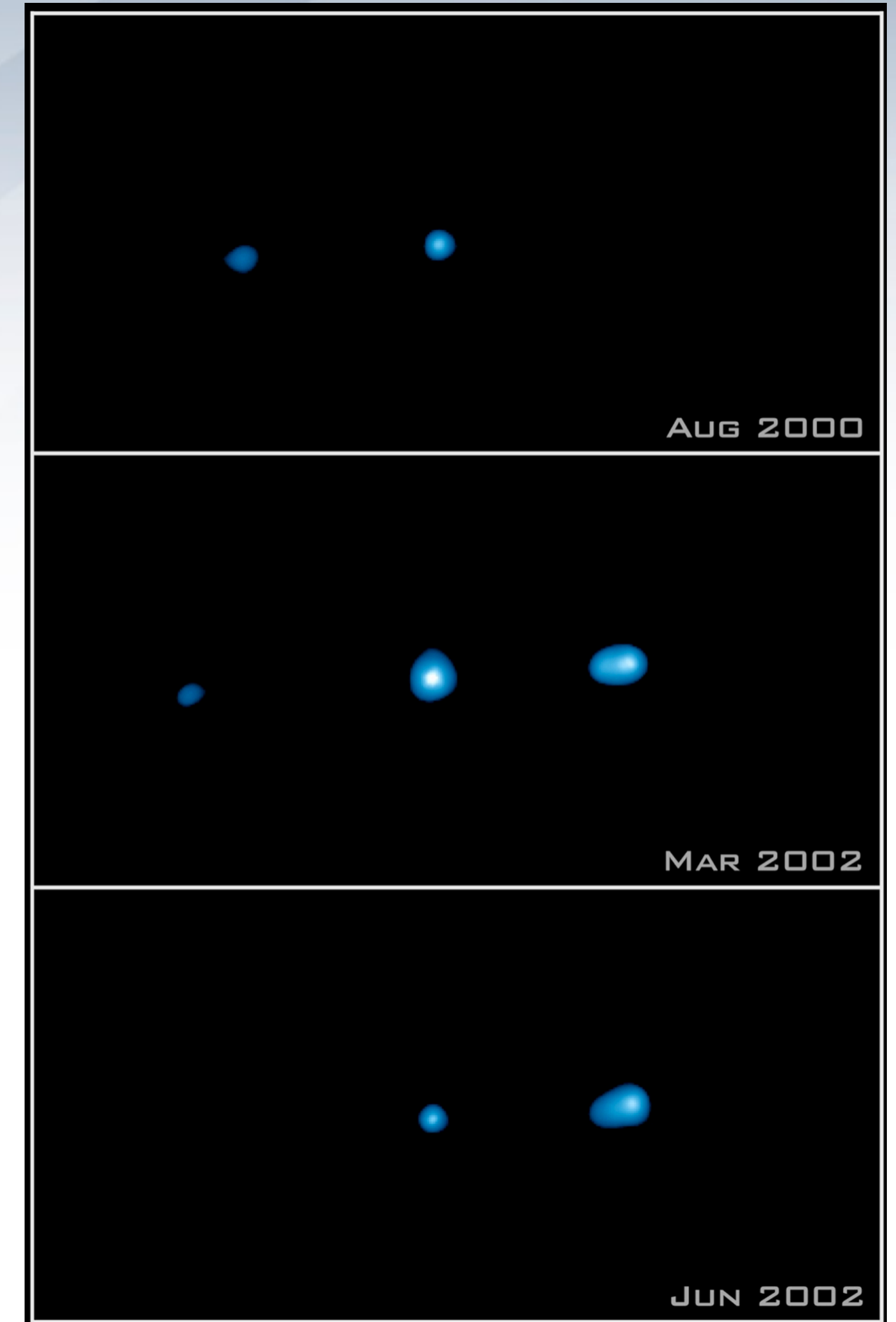
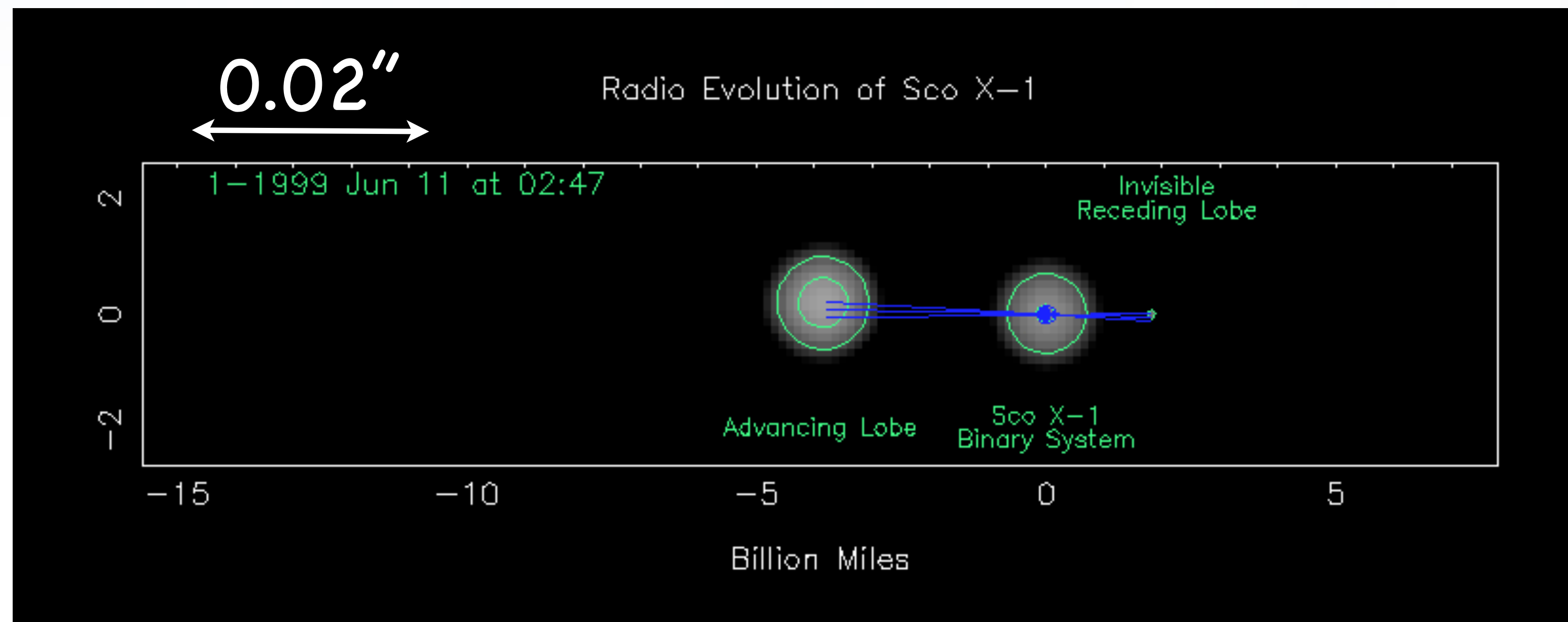
- Development needed
 - Substrate stiffness for 1g testing $\Rightarrow$ Zerodur, 1 cm thick
 - Detector: 1-2 μ imaging resolution
 - X-ray testing of optics: 2 μ source at 500 m = 0.8 mas
 - Optics placement and attitude
 - need 1 m optical mirror! $\Rightarrow$ embed X-ray mirror
 - optical feedback for active focus/pointing control
 - Optical bench metrology for other missions
 - 2 year development to high TRL for stage 1
 - 5 year development for stage 2
- Roadmap toward a Micro-Arcsecond X-ray Imager
 - Need a “finder/guide scope” with larger field of view
 - Establish an X-ray reference frame

X-rays from AGN



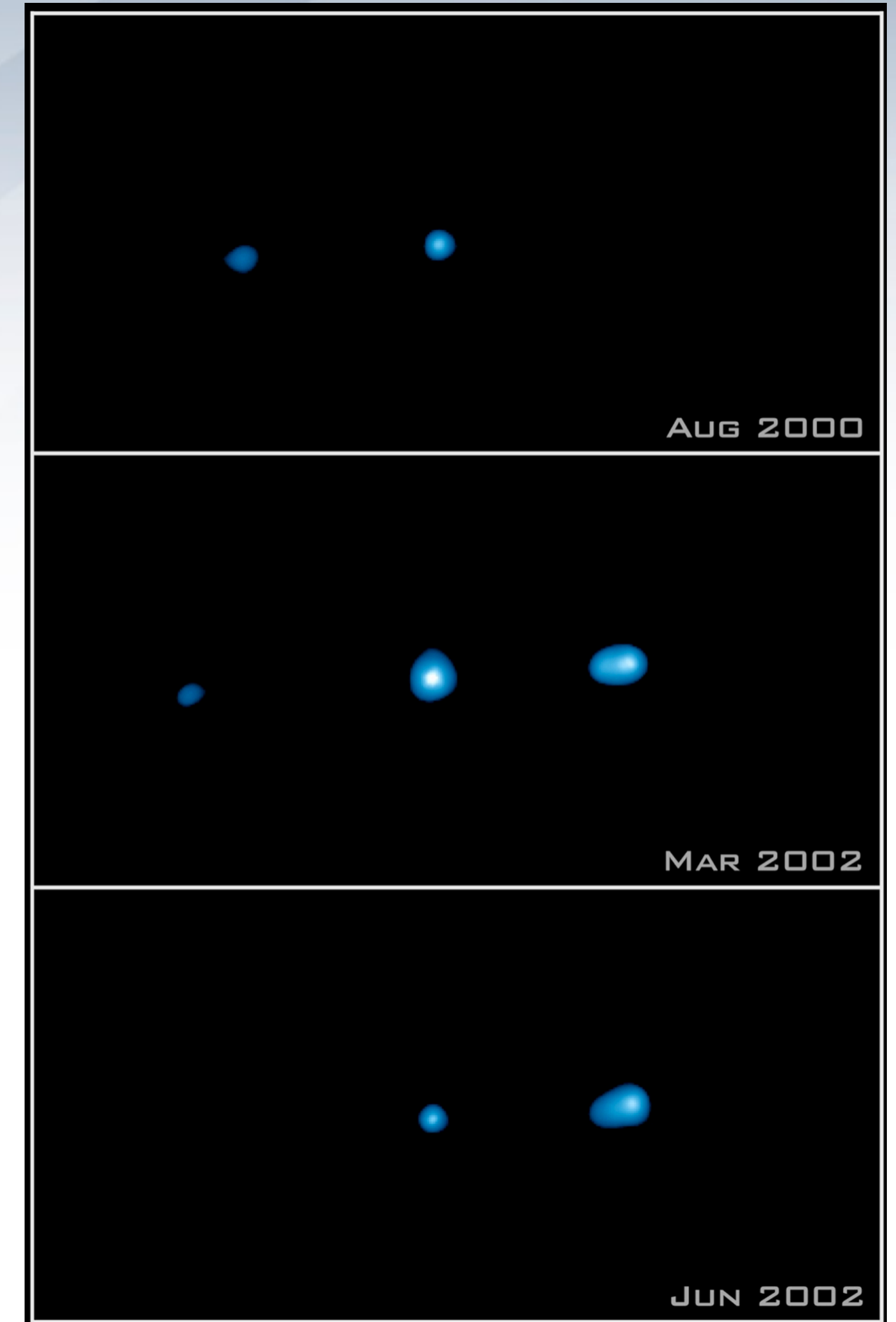
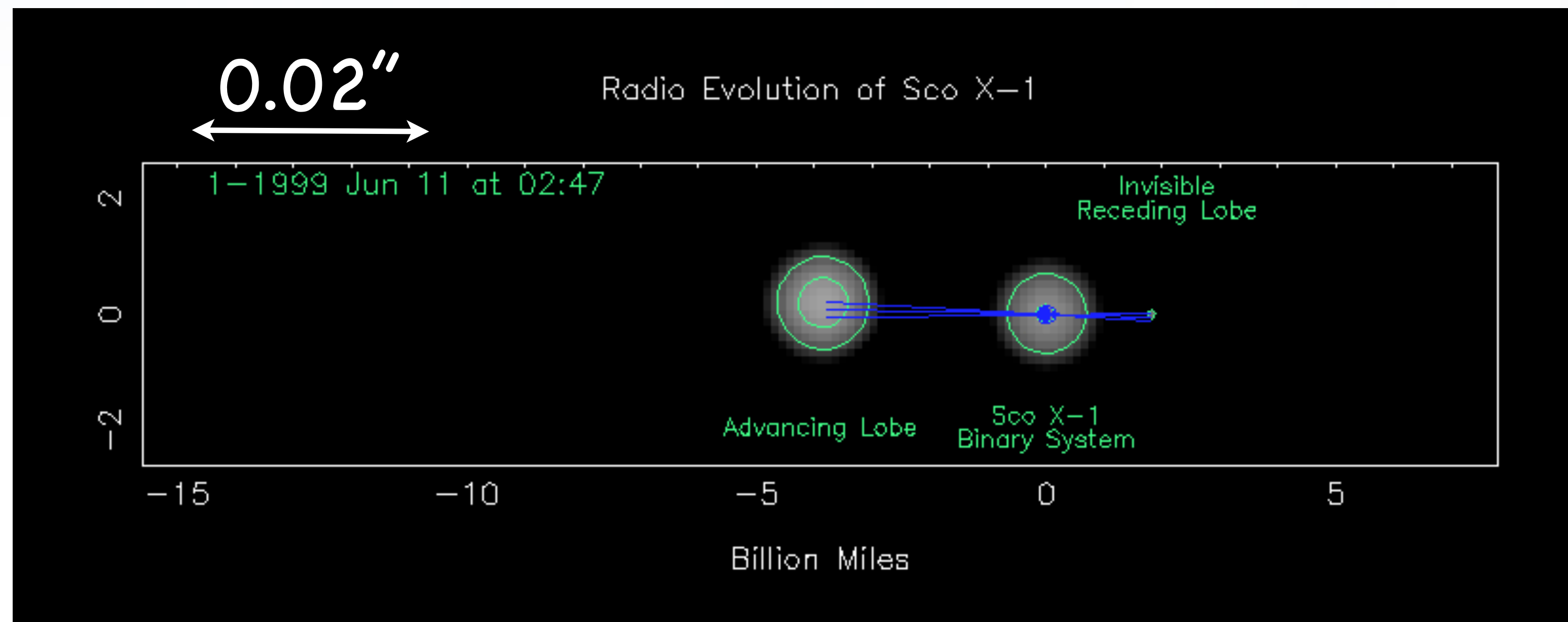
X-ray Binary Jets

- X-ray jets discovered using Chandra
- Proper motion observed — speeds are relativistic
- Radio maps of Sco X-1 indicate high speed knots at 10-30 mas scales

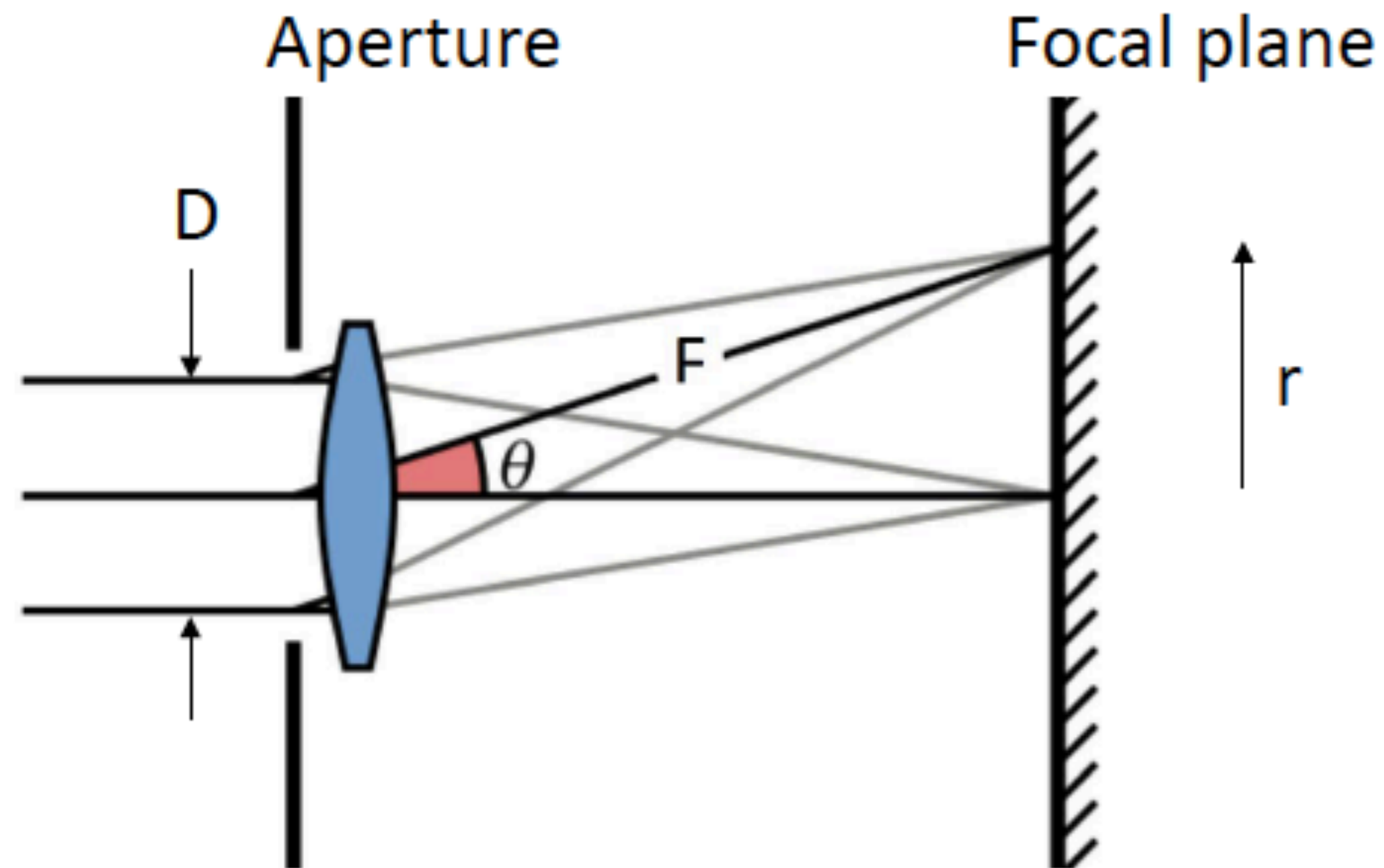


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PSF of a Diffraction Limited Telescope



A diffraction-limited telescope will generate a point spread function (PSF) at the focal plane described by an *Airy disk*

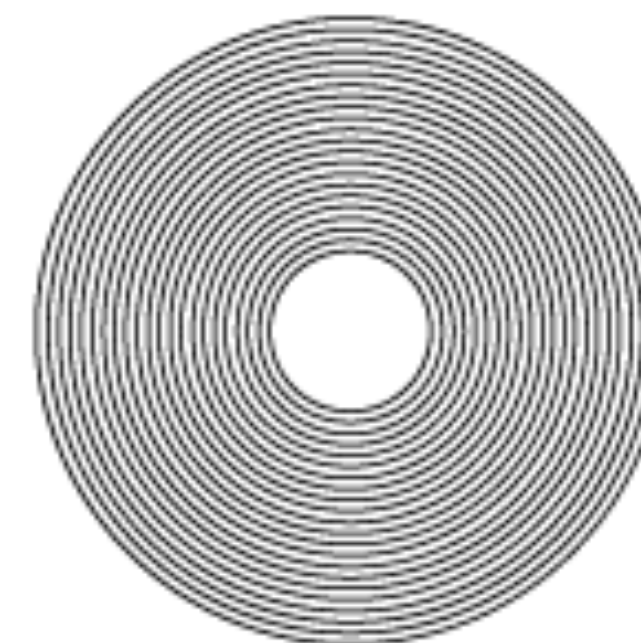
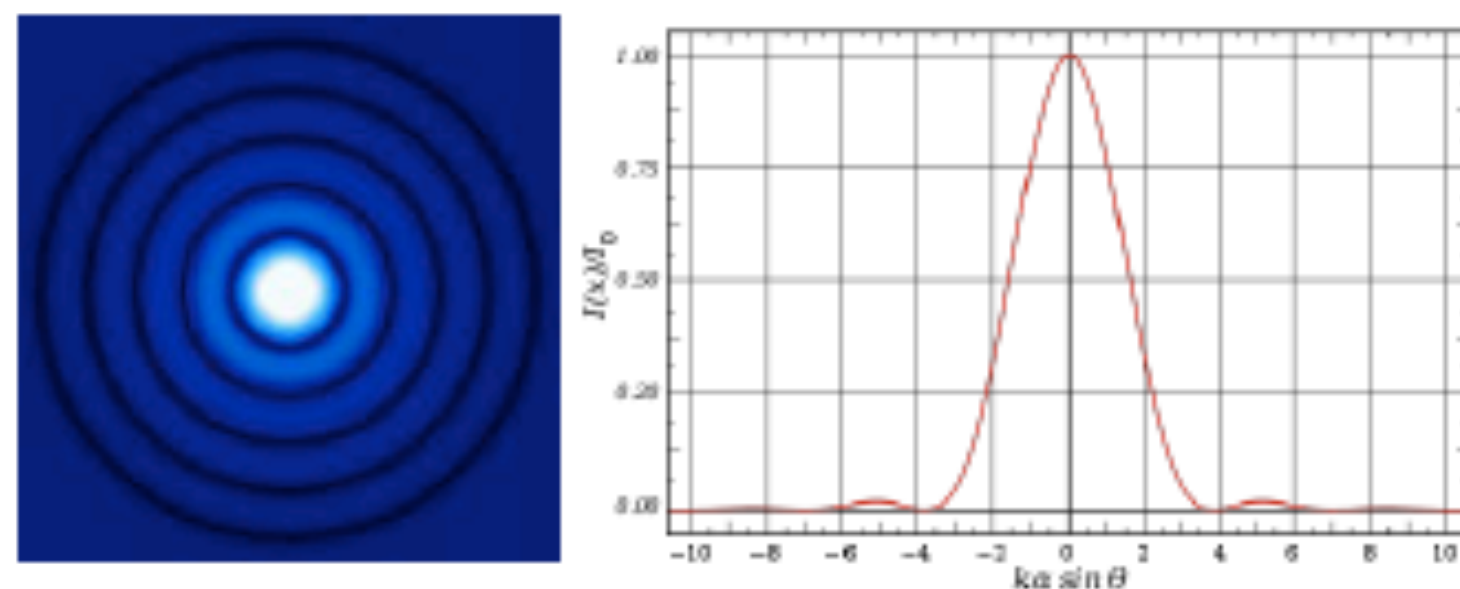
$$I(\theta) = I_0 \left(\frac{2J_1(x)}{x} \right)^2,$$

where J_1 is a Bessel function, $x = k \frac{D}{2} \frac{r}{F}$, $k = 2\pi/\lambda$, D is the aperture diameter, F is the focal length, and $r = F \sin \theta$ is the radial observation point at the focal plane.

The disk's half power diameter (HPD) is given by

$$\text{HPD} \cong \lambda/D$$

Airy disk

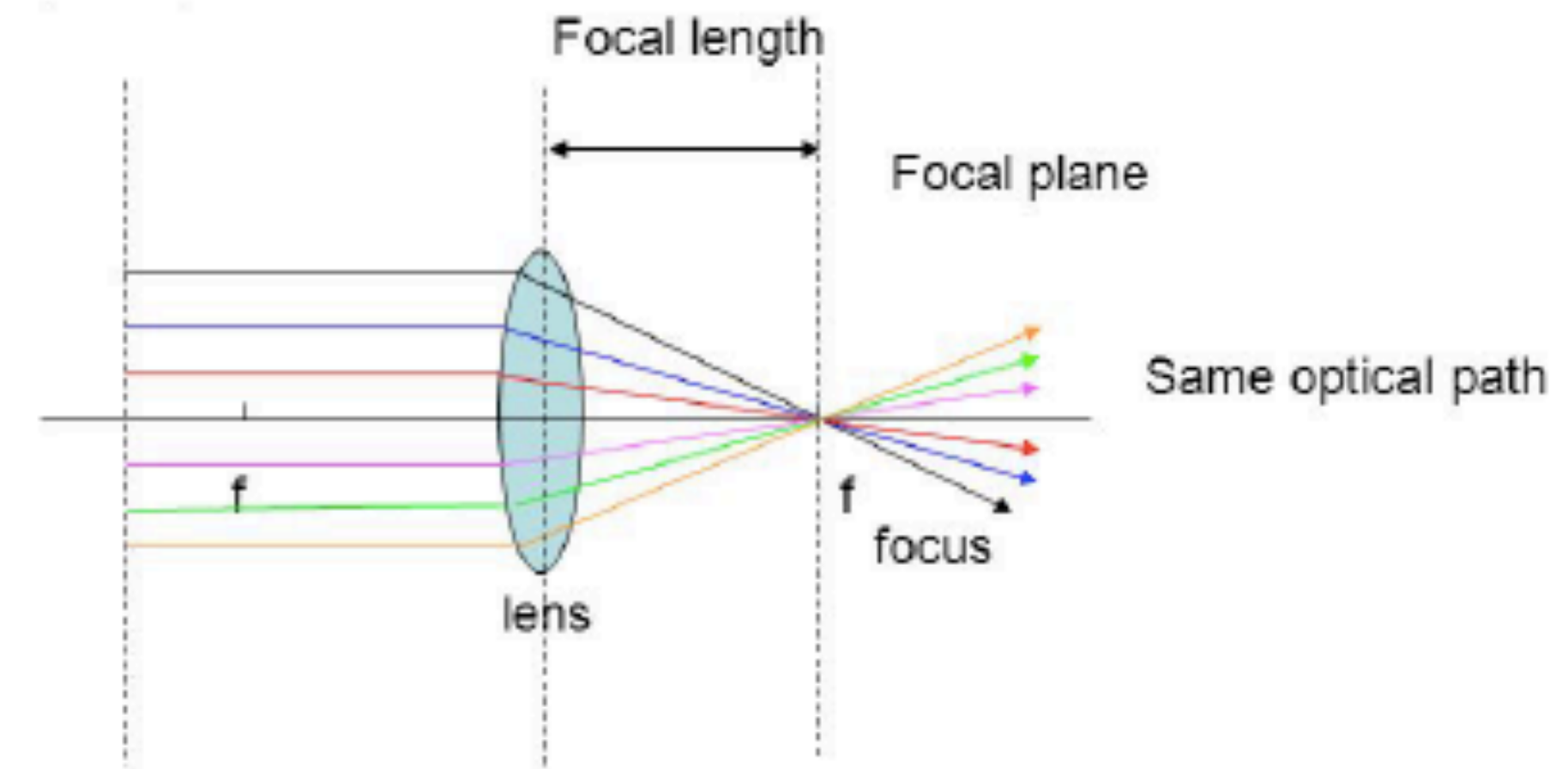


For an “annulated” aperture the telescope HPD is only mildly degraded

Fermat's Principle

- Telescope figure must be “perfect,” which enables ...
- All waves through the telescope aperture to arrive in-phase at telescope focus with a tolerance of $<2\pi/10$
- In other words, the optical path difference (OPD) of all rays from source to focus need to be identical to a small fraction of the λ , i.e., $OPD < \lambda/10$
- At 5 keV, $\lambda = 0.2$ nm, $\lambda/10 = 20$ pm

Fermat's Principle

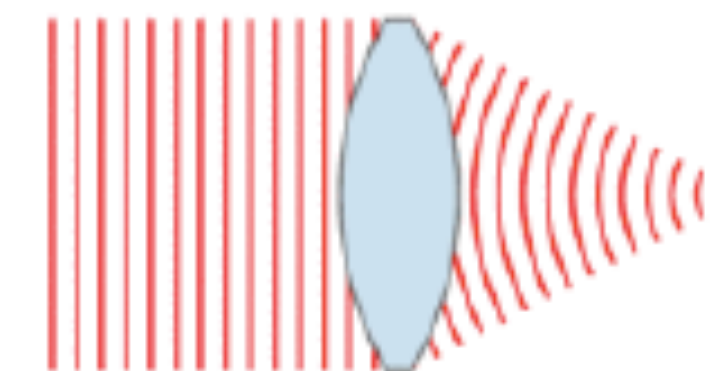


Pierre de Fermat
(1607 – 1665)

Diffraction limited resolution requires all rays to have the same optical path length

$$OPL = \int_a^b n(z) dz$$

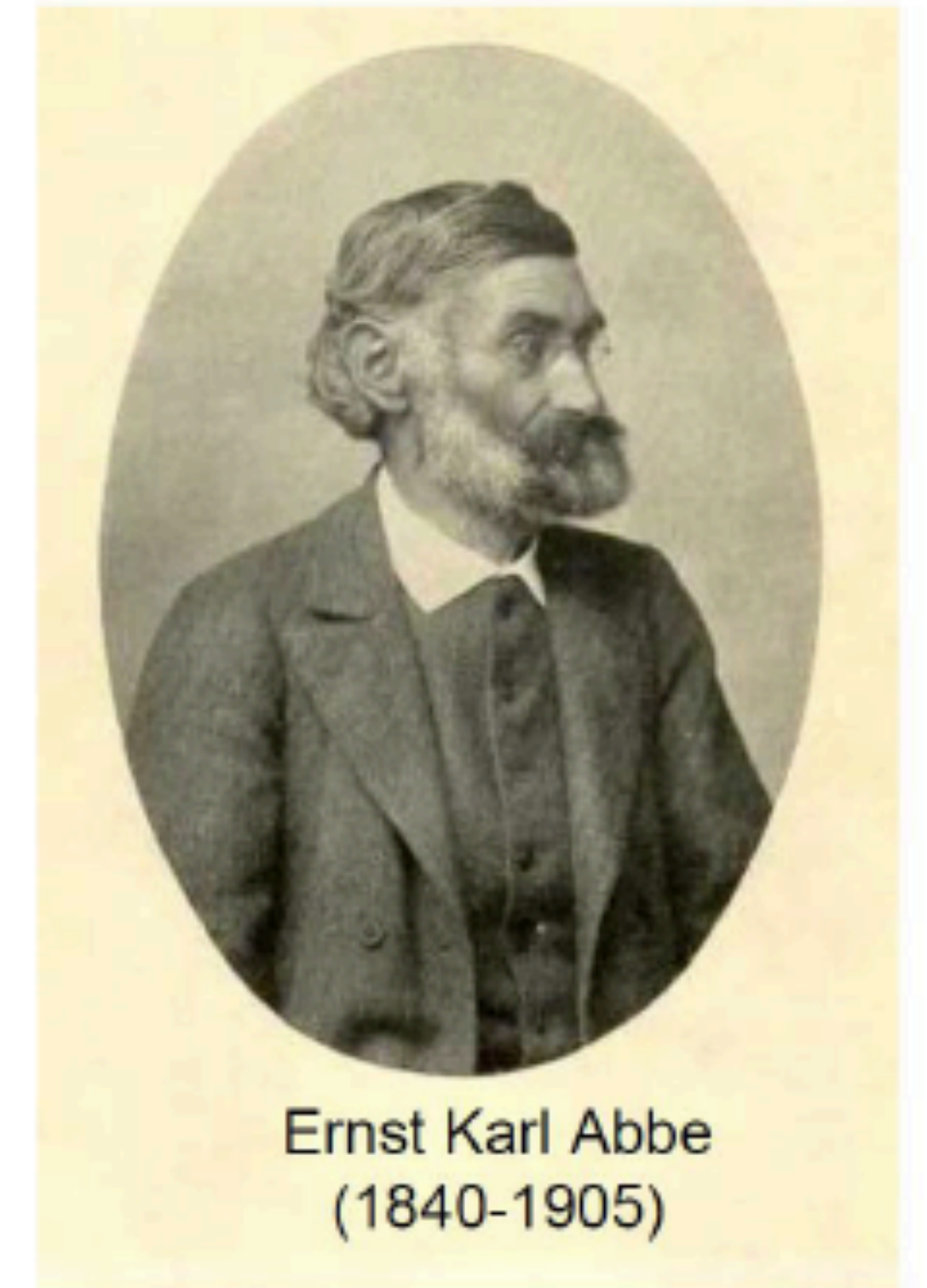
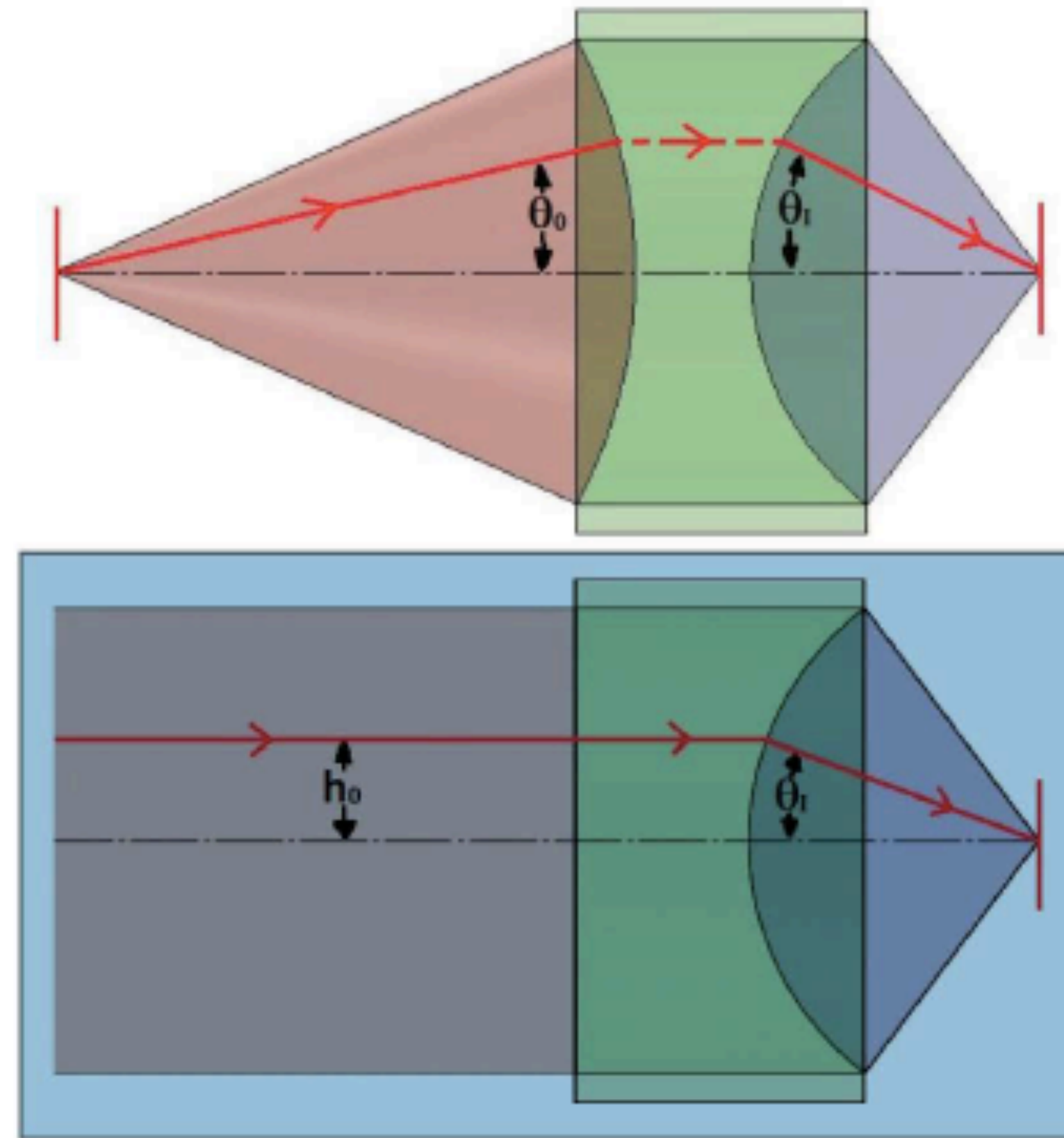
where $n(z)$ is refractive index



All waves must arrive in phase at the focal plane

Abbe Sine Condition

- Enforces constant telescope magnification across the aperture
- Eliminates first-order spherical and coma aberration (aplanatic)



Ernst Karl Abbe
(1840-1905)

Coma free images as long as

$$\frac{\sin \theta_o}{\sin \theta_I} = \text{Constant}$$

for all rays

$$\frac{h_o}{\sin \theta_I} = \text{Constant}$$

Matching Mirror Shell Path Lengths

- There are two parameters common to all shells: $\Delta s, f$
- There are five design parameters for each shell: h_0, L, h_2, z_2, i_0
- Typically h_0 is chosen as the independent variable.

There are three equations (derived from Saha 1987, simplified for P-H telescope) that connect the four design parameters:

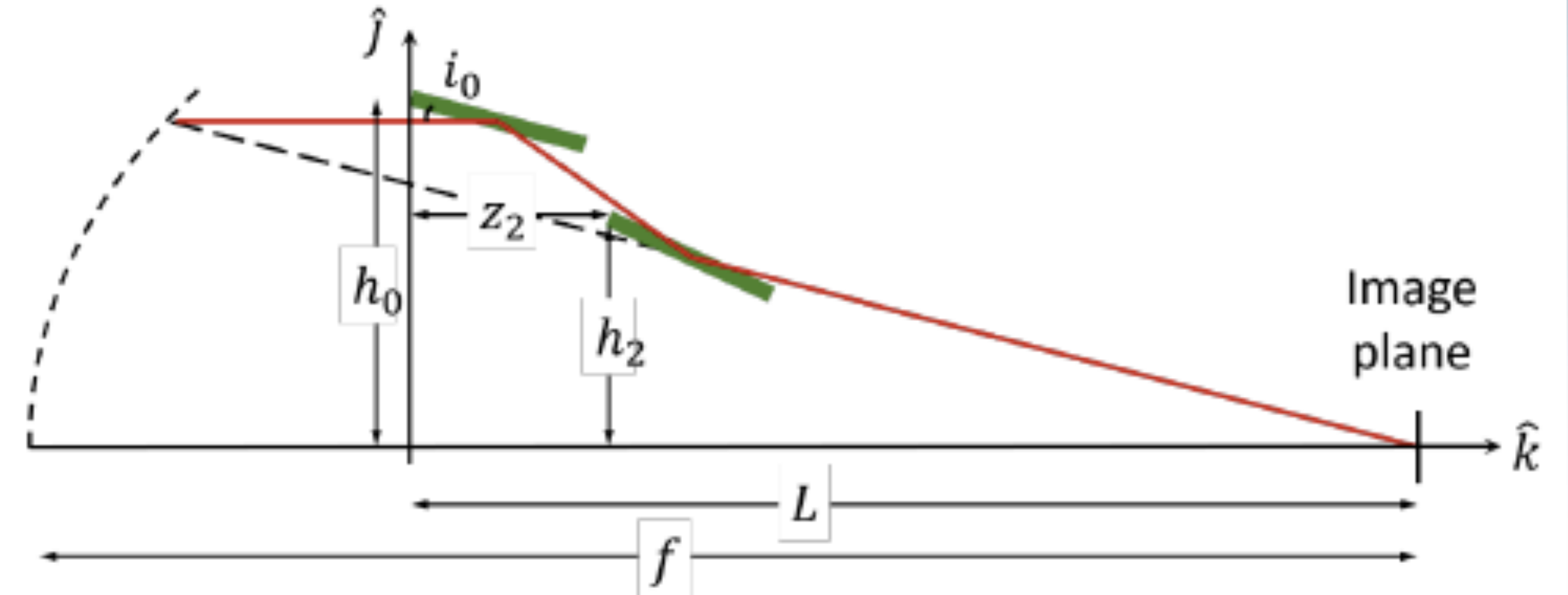
$$\Delta s = \sqrt{(h_0 - h_2)^2 + \left(L - \frac{h_2 f}{h_0} \left(1 - \frac{h_0^2}{4f^2} \right) \right)^2} + \frac{h_2 f}{h_0} \left(1 + \frac{h_0^2}{4f^2} \right) - L$$

$$\tan i_0 = \frac{2f\Delta s - h_0^2}{(2f - \Delta s - 2L)h_0}$$

$$h_0 - h_2 = z_2 \tan 2i_0$$

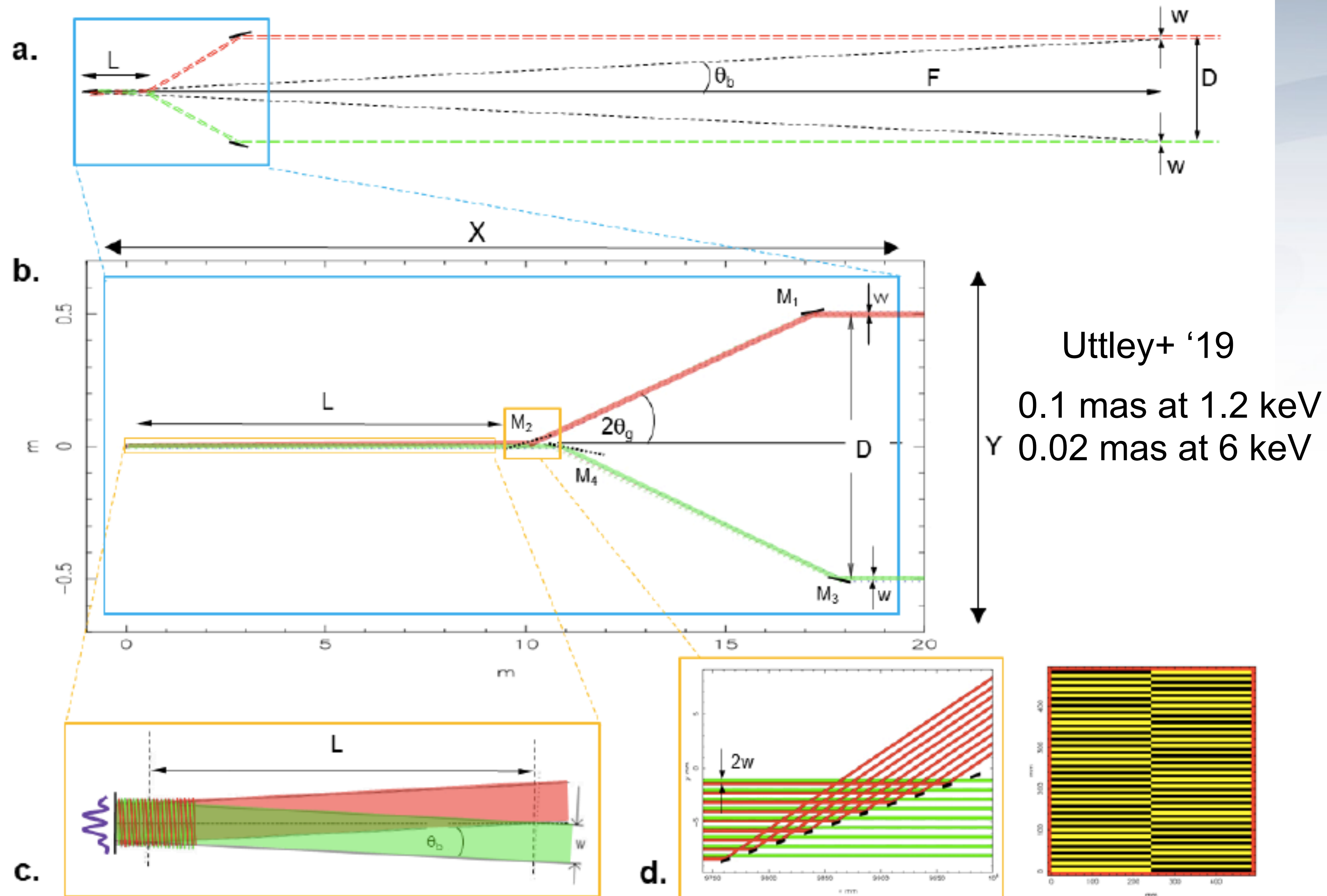
Determining Δs requires choosing two design parameters of a reference shell. The length of a shell with z_2^* and i_0^* is approximately,

$$L^* = f \left(1 - \frac{z_2^*}{h_0^*} \tan 2i_0^* \right) + z_2^* \quad (* \text{ indicates parameter of ref. shell})$$

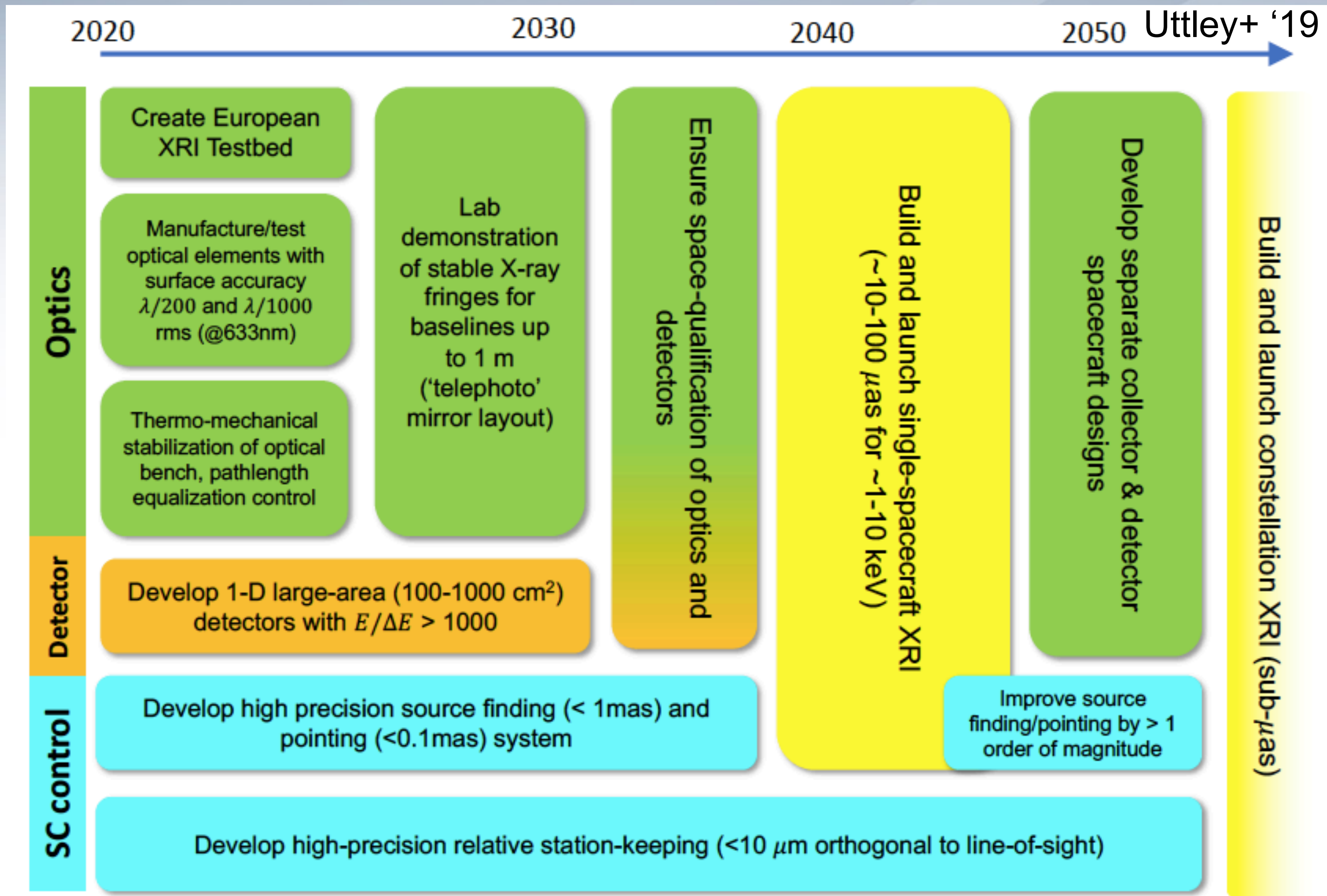


- There is one free design parameter.
- These equations can be solved and evaluated exactly using a symbolic solver and quad-precision arithmetic (since f is large and Δs is small).
- Approximate solutions provide intuition and capture trends.

A Michelson X-ray Interferometer (XRI)



ESA 2050 Vision Roadmap





Diffraction Limited Aspherical Optics Are Critical to the Success of EUV Lithography



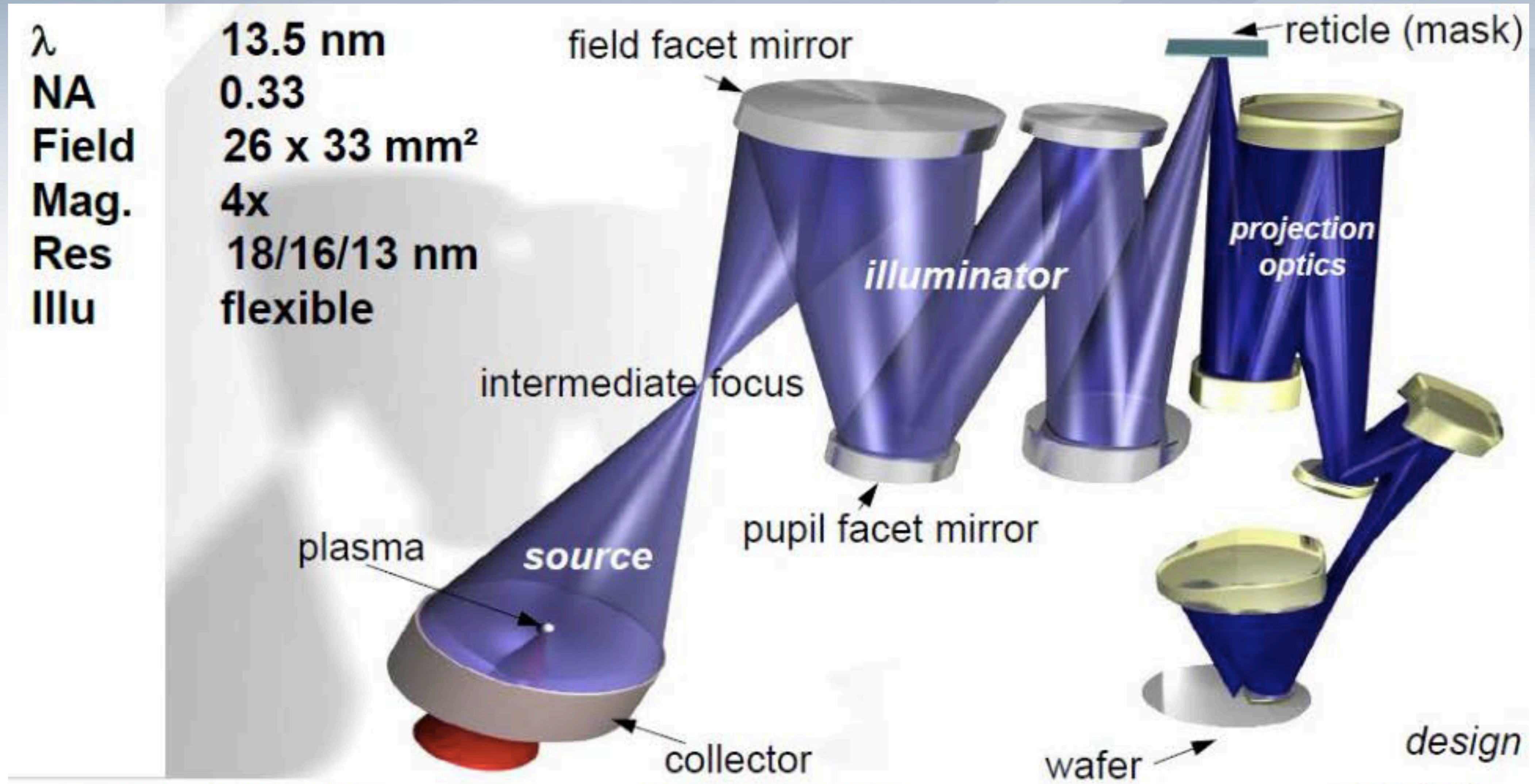
- $\lambda_{\text{EUV}}/50$ figure
- Low flare
- Ultrasmooth finish
- 10 μm departure from a sphere



Tinsley Sample C
Zerodur-M
150 mm diameter

Courtesy of John Taylor, LLNL.

Current Status of EUV Lithography



Carl Zeiss SMT GmbH, Winfried Kaiser

EUVL Symposium 2015 Maastricht

October 7th, 2015